



Advanced Ventilation and Filtration Strategies for Indoor Air Quality and Thermal Comfort

T4.1 development and validation of multi-zone ventilation and thermal comfort model

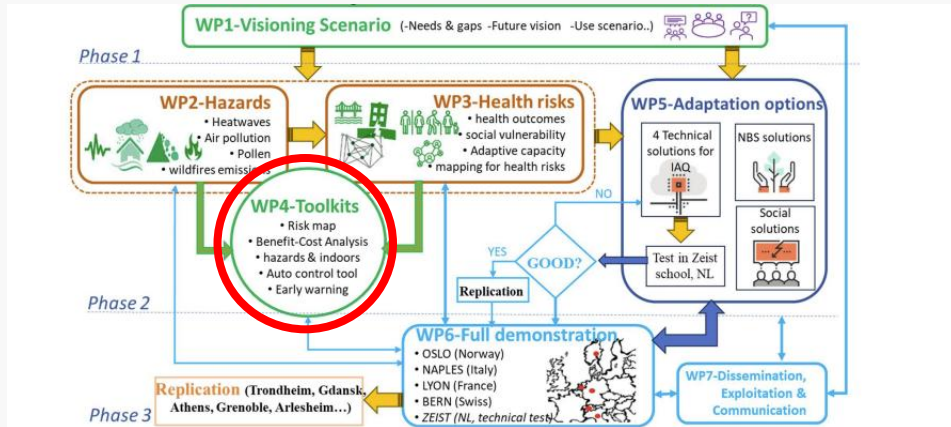
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Health riskADAPT

Coordinator: NILU (Oslo, NO)

Health riskADAPT- User-driven Health risk Assessment Services and Innovative ADAPTation options as Transformative Solutions against Threats from Heatwaves, Air Pollution, Wildfire Emission and Pollen



Goal of the study: simulation and validation of indoor PM2.5

Indoor PM2.5 depends on:

Mechanical ventilation:

- ▶ Ventilation system flow
- ▶ Filtering of outdoor air

Infiltration:

- ▶ Outdoor wind speed
- ▶ Cp pressure coefficients
- ▶ Airtightness of the dwelling
- ▶ Windows open or closed
- ▶ Thermal driving forces (stack effect)

Indoor sources (smoking, cooking, candles)

Indoor deposition & filtering

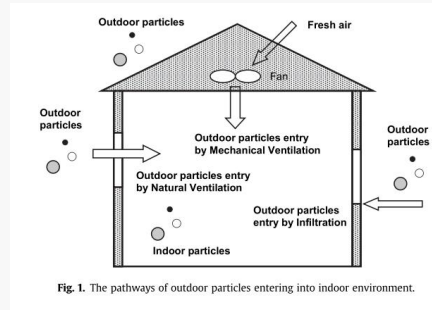


Fig. 1. The pathways of outdoor particles entering into indoor environment.

C. Chen, B. Zhao / Atmospheric Environment 45 (2011) 275–288

PM_{2.5} mass balance for each zone

$$\frac{dC_{in}}{dt} = F \cdot (1 - E_f) \cdot C_o + I \cdot P \cdot C_o - (F + I + k) \cdot C_{in} + \frac{S}{V}$$

- ▶ C_{in} indoor particle concentration ($\mu\text{g}/\text{m}^3$)
- ▶ F ventilation flowrate (m^3/s)
 - ▶ E_f filtration efficiency (-)
- ▶ C_o outdoor particle concentration ($\mu\text{g}/\text{m}^3$)
- ▶ I infiltration flowrate (m^3/s)
 - ▶ P penetration factor (-)¹
- ▶ k deposition rate on indoor surfaces (m^3/s)¹
- ▶ S indoor particle generation ($\mu\text{g}/\text{s}$)
- ▶ V zonal volume (m^3)



Ventilation unit with heat recovery in all 4 dwellings

Ventilation F and infiltration I estimated by CO_2 measurements

¹ penetration factor = 0.73, deposition rate = 0.4 ACH based upon H. Zhao and B. Stephens, "Using portable particle sizing instrumentation to rapidly measure the penetration of fine and ultrafine particles in unoccupied residences," *Indoor Air*, vol. 27, no. 1, pp. 218-229, 2017

PM2.5 and ventilation monitoring and modelling of 4 dwellings: 3 Wezep and 1 Delft



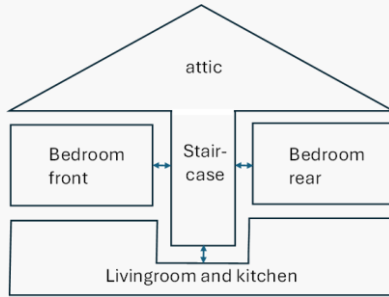
Window open/closed contact



PM_{2.5}, CO₂, RH & T
AirVisual Pro sensor



Occupant presence based on PIR movement sensor



Delft (1)



Wezep (3)

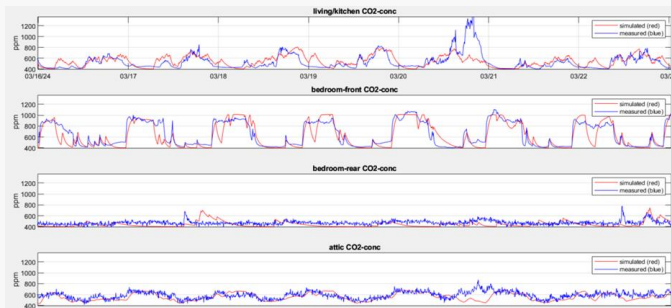
GA No: 101157458
HORIZON-MISS-2023-CLIMA-01-03



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Estimate combined ventilation and infiltration flow per zone over 1 year

- ▶ Source strength Adults 19 dm³ CO₂/h
- ▶ Source strength Children 13 dm³ CO₂/h



The combined mechanical and infiltration flow is used to simulate the indoor PM 2.5 with TNO's AirMAPs: Multizone Airflow Network Model

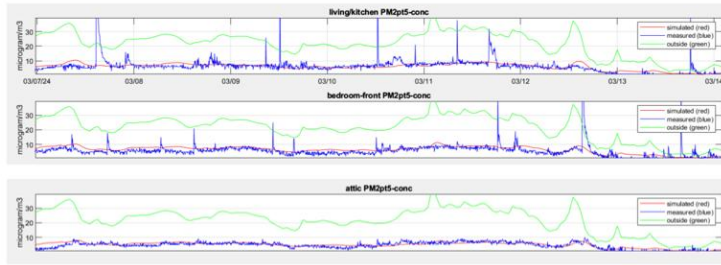
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PM_{2.5} 1 week in March (windows closed)

Delft:
fine F7 filter
 $E_f = 70\%$ (PM_{2.5})
(ePM1 55%)



Underestimation in sim

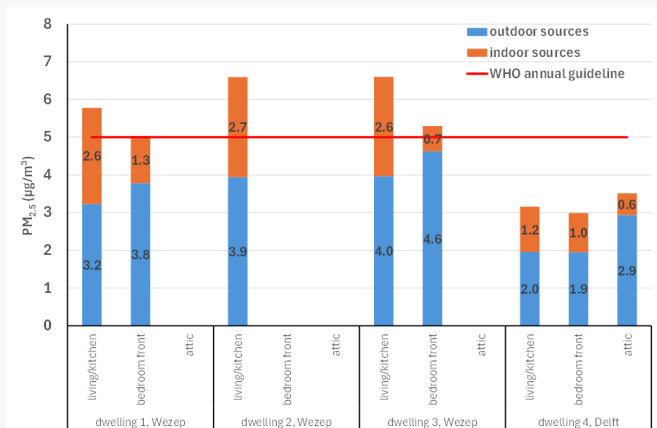
Wezep: coarse
G3 filter
 $E_f = 10\%$ (PM_{2.5})
(about ISO
Coarse 50%)



- Underestimation in simulations possible due to:
- estimated airtightness
 - estimated outdoor CO₂ level
 - unknown particulate matter sources (small sources over a longer period)

Simulated indoor PM_{2.5} values follow measurements except of intermittent indoor sources

With fine filter PM_{2.5} below WHO annual



Coarse G3 filter

| fine F7 filter

F7 filters costs about 20 Euro annual more then G3

Conclusions

- ▶ The simulated CO₂-levels show a moderate to good agreement with the measured values
- ▶ The simulated PM_{2.5} levels (excluding indoor sources, because those are not simulated) correspond reasonable to the measured levels
- ▶ Be aware of correct assumptions on airtightness and outdoor CO₂ levels an unknown particulate matter sources (small hard to detect sources over a longer period)
- ▶ For the dwellings with G3 filter the yearly average PM_{2.5} levels are equal or higher than maximum values recommended by the World Health Organization (WHO)
- ▶ For the dwelling with F7 filter the recommended level is not exceeded.

Next steps towards November 2028

- ▶ Effect of high High-efficiency particulate filtration filter on indoor PM_{2.5}
- ▶ Long term health care building – nursing home
- ▶ More focus on thermal modelling, address combined heat and pollutant stress.

This integrated approach supports evidence-based design for resilient, low-energy buildings that safeguard occupant health under evolving environmental challenges.