APPLICATION OF NUMERICAL SIMULATION IN ASSESSMENT OF MICROCLIMATIC CONDITION IN URBAN AREAS

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ABSTRACT

The proposition of an assessment method of wind condition in urban structures is presented in the paper. In the second part of the paper two virtual residential districts with different urban organisation have been investigated. An assessment model used to examine wind conditions in selected urban organisation structures defines quantitative and qualitative features of the study area. Two elements of the urban environment, wind conditions and urban development, are evaluated. Meteorological data analysis and simulation methods are used to determine individual parameters.

In order to predict wind flow patterns around buildings numerical simulation based on the K - ϵ turbulence model has been used. Application of this method allows for determination the size of the zones with different levels of influence on pedestrian comfort and ventilation as well as enables assessment of microclimatic condition in existing or designing urban complex.

KEYWORDS

wind flow, urban structures, microclimate, numerical simulation, method

INTRODUCTION

The external environment, determined by natural conditions, such as the climate or topography, and anthropogenic factors, that is urban development, the density of urban structures or the size of green areas, has a major impact on living conditions. Dense urban structures in city areas affect unique microclimatic conditions that greatly influence residents' comfort. Local problems connected with excessive air flow in the vicinity of buildings or the formation of strong turbulences may arise in some situations. At the same time, groupings of tall, concentrated buildings sometimes cause a significant decrease in urban ventilation. This may lead to the deterioration of hygienic conditions encourage and accumulations of snow or pollution. The ventilation degree of urban areas also depends on climatic conditions of individual residential districts as they may enhance or counteract the influence of urban development. The knowledge of environmental conditions and the appropriate application of the assessment results greatly contribute to increasing

residents' living comfort. The importance of a comfortable and safe wind environment in urban areas has been emphasized by a large number of authors. Mechanical effects and thermal effects of wind on people were investigated among others by Murakami and Deguchi (1981), Hunt (1976) Lawson and Penwarden (1975), Melbourne (1978), Gendemer (1978), Isyumov and Davenport (1975). The conclusion from these studies have been used to establish several methods to assess the pedestrian wind comfort (Willemsen and Wisse 2002, Delpech et al. 2005, Bottema 2000).

Assessing environmental impacts on human presence is a complex issue as the consideration of a number of variables that characterise individual occurrences is required. The descriptive method and the model method are used most frequently for these purposes. In the latter, a model that comprehensively characterises environmental functions is constructed. It constitutes a certain physical or mathematical pattern that incorporates the greatest possible number of variables affecting individual occurrences.

An assessment model used to examine wind conditions in selected urban organisation structures is proposed and discussed.

ASSESSMENT MODEL OF MICROENVIRONMENTAL CONDITIONS

The suitability of its elements for defined aspects of human occupation is the basic assessment criterion of the microenvironment. Factors such as the climate or urban development play an important role in this respect (Blazejczyk 1983).

The quantitative and qualitative structure of the external environment may be considered in the assessment of environmental conditions using two models: an exponential function model and a model based on Ohm's law.

In the exponential function model, the function base characterises quantitative features of the environment $y = x^z$, while the index exponent – its qualitative features. The value of the function y ranges between 0 and 1. No favourable features of the environment occur for y = 0, and the ideal state is recorded for y = 1. Values x fall within the range of variable between 0 and 1 whereas z may range between 0 and

 $+\infty$. For the most favourable qualitative features z = 0 the function y equals 1.

In the model based on Ohm's law:

$$y_{i} = \frac{U_{i}}{R_{i}} \tag{1}$$

where:

y_i - value of a given parameter

 U_{i} - potential, treated as favourable features of the environment

 $R_{\rm i}$ – resistance, treated as the conditions that make long-term human occupation difficult or impossible

In accordance with Błażejczyk's conception, who proposed combining both models, accepting the condition $z = y_i^{-1}$ for qualitative features, the assessment model of microenvironmental features has the following form [Kozlowska et. al. 1997].

$$y = \left(\frac{U_x}{R_x}\right)^{\left(\frac{U_z}{R_z}\right)}$$
 (2)

where:

 U_x , R_x – potential and resistance of quantitative features

 U_z , R_z – potential and resistance of qualitative features

Assessment of wind conditions

In the assessment of wind conditions, occurrence frequencies of favourable and unfavourable wind speeds in a given year constitute quantitative wind features. The frequency of weather types favourable for subjective human heat perception is accepted to be potential (U_x) and the frequency of unfavourable conditions to be resistance (R_x) .

$$x = \frac{NA_2 + 0.75NA_3}{1 + NA_1 + N(BC)} \tag{3}$$

where:

 NA_1 , NA_2 , NA_3 – occurrence frequency of wind conditions classified as A_1 , A_2 and A_3

N(BC) – occurrence frequency of wind conditions B and C unfavourable for people in the study period

For the purposes of this assessment, a weather classification based on the subjective perception of various weather types was used. Following the weather typology devised by the Institute of Geography and Spatial Organization, Polish Academy of Sciences, human heat perception caused by the reaction of the thermoregulatory system to atmospheric stimuli (air temperature, wind speed) and the wind's mechanical effect on people were used as the basic features of weather types.

Table 1 Types of wind weather

	\mathbf{A}_1	unfavourable wind		$0 \div 1,0$
		conditions due to		
		decreased aeration		
	A_2	wind conditions		1.0÷3.0
		tolerable for active		
		relaxation and		
Weather type		work, clothes		
		flapping	Wind speed [m/s]	
	A_3	conditions in which		3.0÷5.0
		dust and paper are		
		lifted	bee	
	\mathbf{B}_1	wind force	s p	5.0÷8.0
≥		perceptible on the	Vin	
		body, possible	>	
		tripping		
	B_2 ir	impeded walking,		8.0÷10
		unpleasant sounds		
	С	difficulty in		>10
		controlling walking,		
		difficulty in keeping		
		balance		

Qualitative features of wind conditions may be described by the parameters of the intensity of wind direction changes and the mean participation of the n wind direction. They may be determined using the equation:

$$z = \frac{1 + I_N}{1 + I_K} \cdot \frac{1 + N_N}{1 + N_K} \tag{4}$$

where:

 I_N – intensity of wind direction changes for wind speeds lower than 1m/s and greater than 5m/s

 I_K – intensity of wind direction changes for wind speeds $1 \div 5 \text{m/s}$

 N_N – mean wind participation for wind speeds >5m/s and <1m/s and n wind directions in the study period N_K – mean wind participation for wind speeds $1\div5$ m/s and n wind directions in the study period

The intensity of wind direction changes may be determined from the equation:

$$I_{N} = \frac{1,07\sqrt{\frac{1}{\left(n-1\right)}\sum_{i=1}^{n}\left(N_{Ni} - \left\langle N_{Ni}\right\rangle\right)^{2}}}{\left\langle N_{Ni}\right\rangle} \tag{5}$$

for wind speeds <1 m/s and > 5 m/s

$$I_{K} = \frac{1,07\sqrt{\frac{1}{(n-1)}\sum_{i=1}^{n}\left(N_{Ki} - \left\langle N_{Ki}\right\rangle\right)^{2}}}{\left\langle N_{Ki}\right\rangle}$$
(6)

for wind speeds 1÷5m/s

where:

 N_{Ni} – occurrence frequency of speeds <1m/s and >5m/s for i wind directions in the study period

 N_{Ki} – occurrence frequency of speeds 1÷5m/s for i wind directions in the study period, i = 1,2,...8

$$\left\langle N_{_{N}}\right\rangle =\frac{\displaystyle\sum_{_{i=1}}^{n}N_{_{Ni}}}{n} \qquad \left\langle N_{_{K}}\right\rangle =\frac{\displaystyle\sum_{_{i=1}}^{n}N_{_{Ki}}}{n}$$

Having substituted x, z in the general model, a dimensionless coefficient of wind conditions is obtained:

$$W_{k} = \left[\frac{NA_{2} + 0.75NA_{3}}{1 + NA_{1} + N(BC)}\right]^{\left[\frac{1+I_{N}}{1+I_{K}}, \frac{1+N_{N}}{1+N_{K}}\right]}$$
(7)

Climatic (wind) conditions may be assessed using the categories of the coefficient W_k presented in the table 2.

Table 2 Coefficient of climatic condition assessment

W_{K}	CONDITIONS		
≤ 0.20	unfavourable		
$0.20 \div 0.40$	relatively unfavourable		
$0.40 \div 0.60$	moderate		
$0.60 \div 0.80$	favourable		
≥ 0.80	very favourable		

The above classification is the present author's suggestion. Other quantitative and qualitative parameters may be used instead of the proposed features of weather conditions.

Assessment of urban development

The impact of urban development on microclimatic conditions is assessed using the organisation of a dense urban structure and the range of tall and low vegetation areas. The participation of the open area Z_w in the total surface was considered to be the potential of quantitative features of the land development coefficient Z_t and the participation of various urban structures and green areas in relation to the study area was considered to be their resistance (Z_m). The occurrence of zones for which wind speeds ranged between 1m/s and 5m/s (S_{Ki}) was accepted as the potential of qualitative features and the participation of zones with threatened human balance in the study area and poorly aerated zones (S_{Ni}) for the i direction, $i = 1,2 \dots n$, was accepted as their resistance.

The urban organisation coefficient is as follows:

$$Z_{t} = \left(\frac{Z_{w}}{1 + Z_{m}(1 + R_{zs})}\right)^{\left[\frac{1 + S_{Ni}}{1 + S_{Ki}} ... \frac{1 + S_{Nn}}{1 + S_{Kn}}\right]}$$
(8)

$$Z_{w} = 1 - Z_{m}(1 + R_{zs})$$

Coefficients S_{Ni} and S_{Ki} are determined from the equation:

$$S_{Ni} = \frac{S_{Ni}}{S_o} \int_{w} \int_{v}$$

$$S_{Ki} = \frac{S_{Ki}}{S_o} \int_{w} \int_{v}$$

where:

 S_{Ni} – zone surface with speeds <1m/s and >5m/s, caused by a varied urban structure for i wind direction

 S_{Ki} – zone surface with speeds 1÷5m/s for i wind direction

 \int_{w} – weight factor dependent on the wind direction

 \int_{v} – weight factor dependent on wind speed changes

S_o – surface of the total urban study area

R_{zs} – coefficient of urban structure density

The values of the coefficient Z_t may be grouped depending on the suitability degree of urban development (tab. 3).

Table 3. Coefficient of urban development assessment depending on area suitability

\mathbf{Z}_{T}	URBAN ORGANISATION			
≤ 0.2	unfavourable			
$0.2 \div 0.3$	relatively unfavourable			
0.3 - 0.4	moderate			
0.4 - 0.5	favourable			
≥ 0.5	very favourable			

The classification accepted after K. Błażejczyk's conception in the bioclimatic assessment

Overall assessment of environmental conditions

The overall assessment of environmental conditions may be described by the coefficient B_k expressed by:

$$B_k = \frac{W_k + Z_t}{2} \tag{9}$$

Coefficient values may be classified on the basis of Błażejczyk's conception (tab. 4).

Table 4. Coefficient of the overall assessment of environmental conditions

B_{K}	CONDITIONS
≤ 0.175	unfavourable
0.176 - 0.317	relatively unfavourable
0.318 - 0.459	moderate
0.460 - 0.574	favourable
≥ 0.575	very favourable

<u>APPLICATION OF THE METHOD:</u> EXAMPLE

The wind microclimate of two virtual residential districts was assessed using the above equations. Fig. 1 presents the urban organisation of the districts. Each system consists of six buildings located in the suburban area. Two building types were examined in the systems: 5-storey cubes and 12-storey rectangular prisms. Minimum distances for transport and green areas were designed between the buildings. An area located in Warsaw was analysed. Meteorological data used in the assessment of wind conditions covered the decade between 1976 and 1985.

Quantitative features of wind conditions were determined using the occurrence frequency analysis of individual groups and subgroups of wind conditions. Occurrence frequencies of the A, B and C weather (wind) groups are given in table 5.

Table 5. Occurrence frequencies of wind weather groups

OCCURREN	WEATHER GROUPS					
CE	A_1	A_2	A_3	B ₁	B ₂	C_1
FREQUENCI	WIND SPEEDS					
ES OF WIND GROUPS	0-1	1-3	3-5	5-8	8-10	>10
NA ₁	0.10					
NA_2		0.36				
NA_3			0.31			
NB ₁				0.19		
NB_2	•				0.02	
NC ₁						0.02

Using the equations from $3 \div 7$ and the determined occurrence frequencies of wind weather types, the dimensionless assessment coefficient of wind conditions, $W_k = 0.66$, was calculated.

Urban development was assessed next. Urban structures with constant urban development value $S_{\rm o}=3360 m^2$ were considered. The surface of the area studied was a circle with the radius $R_{\rm o}=140 m$. Coefficients $S_{\rm Ni}$ and $S_{\rm Ki}$ describing the participation of zones with threatened human balance and poor ventilation and zones for which wind speeds ranged between 1m/s and 5m/s were determined in numerical simulations of the air flow around the analysed urban systems.

Numerical simulation

The numerical analysis of wind flow around the analysed buildings has been developed with the aid of the standard $k - \varepsilon$ model proposed by Launder and Spalding (1974). The governing equations were the time-averaged, momentum, continuity, and the $k - \varepsilon$ model equations.

On the surfaces of the building and the ground, the wall function method by Launder & Spalding (1974) is used to prescribe the boundary conditions for velocity and turbulence quantities, assuming that the

turbulence is in the state of local equilibrium. At the outlet boundaries, all the quantity gradients are zeros except the velocity component of z direction.

In the inlet of the computation domain logarithmic mean wind profile including change of the roughness parameters has been established (Fig.1.) As the reference wind speed $V_1 = 5 \text{m/sec}$ (at an altitude of 10 m above the ground level) has been assumed. Using a simple relation proposed by Simiu (1986) wind velocity profile at the reference site (meteorological station) has been linked with the profile over the analysed terrain assuming that gradient wind velocity is constant.

$$\frac{V_1 *}{V_2 *} = \left(\frac{Z_{o1}}{Z_{o2}}\right)^{0.0706} \tag{9}$$

where:

 V_1 * = friction velocities for the reference site;

 V_2 * = friction velocities for the analysed terrain;

 z_{o1} = aerodynamic roughness length of the reference site (0.03 m);

 z_{o2} = aerodynamic roughness length of the analysed terrain (0.25 m).

Turbulence kinetic energy and dissipation rate profiles have been derived from the equations:

$$K = \frac{3}{2}(VI) \tag{10}$$

where:

I- turbulence intensity assumed to be equal to 15%

$$\varepsilon = C_{\mu} \frac{K^{\frac{3}{2}}}{1} \tag{11}$$

where: 1 = 0.4z.

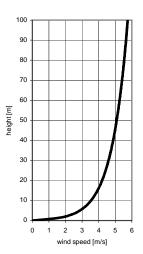


Figure 1. Wind profile

Taking into account the updated Davenport classification (Wieringa 1992) roughness length $z_{\rm o}$ for inflow has been assumed at 0.25m (for rural area). Building roughness was taken as 0.002m. The dimensions of the computational domain differ in accordance with direction of approaching flow. For example in the case of west wind direction W,L,H = 535 x 468 x 160m.

Unstructured tetrahedral grid has been generated with a total of over 2 million cells. A higher mesh density has been defined in the vicinity of the buildings.

Numerical analysis have been done for 8 wind directions. As the wind speed at pedestrian level were crucial the analysis has been limited to a level of 1.8m (pedestrians level).

Application of numerical simulation allowed to determine size of the zones with different influence on wind climate. In relatively short time analysis of wind flow around different configurations of the buildings and different wind direction were carried out. Figures $2 \div 7$ illustrate some examples of wind speed distribution around two building's systems.

Obtained results formed the basis for determination of potential and resistance of qualitative features and in consequence the urban development coefficient. The next step was overall assessment of environmental condition. Table 6 presents values of basic factors and results of assessment.

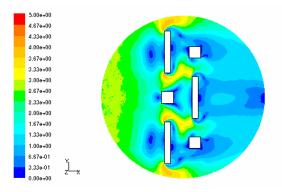


Figure 2. Wind speed distribution for west wind direction. system I

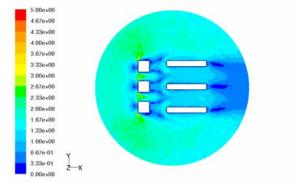


Figure 3. Wind speed distribution for west wind direction. system II

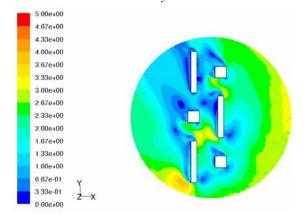


Figure 4. Wind speed distribution for east wind direction. system I

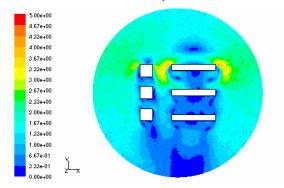


Figure 5. Wind speed distribution for northt wind direction. system II

CONCLUSION

The proposition of an assessment method of wind condition in urban structures is presented in the paper. In the second part of the paper two virtual residential districts with different urban organisation have been investigated. In order to predict wind flow patterns around buildings numerical simulation based on the K - ϵ turbulence model has been used. Application of this method allows for determination the size of the zones with different levels of influence on pedestrian comfort and ventilation. The overall assessment of environmental condition based mainly on wind parameters demonstrated that in the case of system I wind condition can be described as favourable. The urban organisation cause wind speed acceleration,

especially near the corners of the buildings and thereby improve ventilation process. The second system is characterised by moderate condition. This is caused mainly by lower wind speed values comparing with previous system. The above conclusions are valid only for assumed approaching wind velocity. In order to draw a more general conclusion wind speed should be consider as amplification factor y. Application of the above method allows for initial comparison of different urban structures in order to create the comfortable environment for residents. However this proposition refers only to wind condition. Assessing environmental impacts on human presence is a complex issue as the consideration of a number of variables that characterise individual occurrences is required. In the future works more elements will be take into the consideration.

REFERENCES

- Blazejczyk K. 1983. "Bioclimatic assessment and typology of Polish health resorts," Dokum. Geogr., IGiPZ PAN, 3 Warsaw (in polish)
- Bottema M. 2000. "A method for optimization of wind discomfort criteria", Building and Environment, vol. 35, pp.1-18
- Delpech P., Baker C.J., Blackmore P.A., Koss H., Sanz-Andres A., Stathopoulos T., Willemsen E. 2005 "Pedestrian wind comfort assessment criteria: A comparative case study", EACWE4 The 4th European & African Conference on Wind Engineering, J.Náprstek & C.Fischer (eds.): ITAM AS CR, Prague
- Gandemer J. 1975. "Wind environment around buildings: aerodynamic concepts", Proc. of the 4-th International Conference on Wind Effects on Buildings and Structures, Heathrow, pp.423 -432
- Hunt J.C.R., Poulton E.C., Mumford J.C., 1976. "The effects of wind on people; New criteria based on wind tunnel experiments", Building and Environment, vol.1, pp.15-28
- Isyumov N., Davenport A.G., 1975. "The ground level wind environment in built-up areas", Proc. of the 4-th International Conference on Wind Effects on Buildings and Structures, Heathrow
- Kozlowska-Szczesna T., Blazejczyk K., Krawczyk B. 1997. Human Bioclimatology. Methods and applications. IGiPZ PAN ,Warsaw, 200 pages (in polish)
- Launder B.E. and Spalding D.B. 1974. "The numerical computation of turbulent flows,". Computer Methods in Applied Mechanics and Engineering 3, pp.269-289

- Lawson T.V., Penwarden A.D., 1975. "The effects of wind on people in the vicinity of buildings", Proc. 4 th Int. Conf. on Buildings and Structures, Heathrow, UK, pp.605-622
- Melbourne W.H., 1978. "Criteria for environmental wind conditions", Journal of Wind Engineering and Industrial Aerodynamics, 3, pp.241-249
- Murakami S., Deguchi K., 1981. "New criteria for wind effects on pedestrians," Journal of Wind Engineering and Industrial Aerodynamics 7, pp.289-309
- Simiu E. and Scanlan R.H. 1986. Wind effects on structures. New York: John Wiley & sons, 590 pages
- Wieringa J. 1992. "Updating the Davenport roughness classification," Journal of Wind Engineering and Industrial Aerodynamics, 41-44, pp. 357-368
- Willemsen E., Wisse J.A., "Accuracy of assessment of wind speed in the built environment," Journal of Wind Engineering and Industrial Aerodynamics, 90, pp.1183-1190

Table. 6. Values of basic factors

URBAN STRUCTURE (VARIANT)	PERCENTAGE OF URBAN STRUCTURES AND GREEN AREAS IN TOTAL AREA Z _M	STRUCTURE DENSITY COEFFICIENT R _{ZS} (1- R _{SR} /R _O)	URBAN DEVELOPMENT ASSESSMENT COEFFICIENT Z _T	OVERALL COEFFICIENT OF WIND MICROCLIMATE ASSESSMENT B _K	CONDITIONS
I	0,05	0,717	0,59	0,54	favourable
II	0,05	0,802	0,35	0,42	moderate

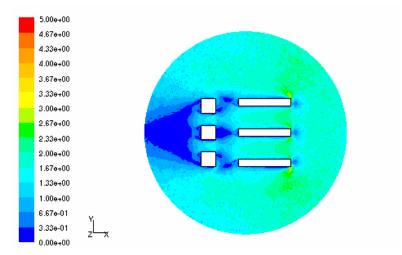


Figure 6. Wind speed distribution for east wind direction. system II

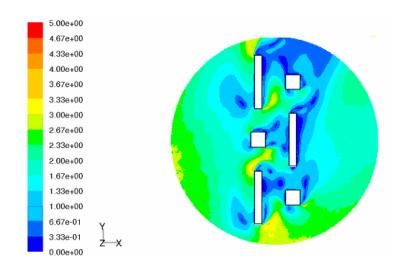


Figure 7. Wind speed distribution for south-west wind direction. system I