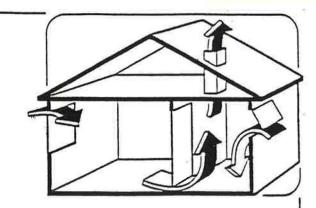
AIVC Workshop on Data base Warwick, GB



Weather and aeraulic data set for validation

The LESO Building

Part. 2
Building description and Measurement report

(March 1990)

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Weather and agrantin data set for validation

The LESO Building

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ABSTRACT

The document presents the LESO Building and its principal parameters as dimensions, air leakage distribution, pressure coefficients and air renewal. This data base is provided to help for one step in the validation of air infiltration simulation codes.

The reference gives associated papers which are necessary for the use of the data set.

INTRODUCTION

This document constitutes the core of the LESO data-set for validation of multi-zone air infiltration models. It describes the building and the test site and report the aeraulic measurements made between 1987 and 1990, according the reporting format described in the AVC tech. note 6.

This document, with the principal papers quoted in references [5, 6, 7, 8, 9,], may allow the use of the data-set. But the authors want to emphasize that, since there is much diffuse information which cannot be included in such a document, a correct use of the data-set and a comprehensive analysis of the results obtained by its use requires a close discussion with the authors.

The floppy disk containing numerical data set is not automatically annexed to this document but is available from the authors. Moreover, it is planned to include the LESO data set in the AIVC data base.

The document is divided in four items:

- 1. General information
- 2. Test site description
- 3. Building description
- 4. Operation and numerical data set.

1. GENERAL INFORMATION

1.1 Country Switzerland.

1.2 Principal researchers J.-M. Fürbringer

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1.8 Title of the project ERL - Task B 3.2.

"Programmes de calcul détaillés et simplifiés des échanges d'air dans le bâtiment : Validation à l'aide de mesures expérimentales" [1, 2, 3].

1.9 Principal objectives

Constitution of a data-set for purpose of validation.

1.10 References

- 1. 1. Status Seminar "Forschungsprogramm: Energierelevante Luftströmungen in Gebäuden", Winterthur, Switzerland, 1987 (French and German).
- 2. Status Seminar "Forschungsprogramm: Energierelevante Luftströmungen in Gebäuden", Lausanne, Switzerland, 1988 (French and German).
- 3. Status Seminar "Forschungs programm: Energierelevante Luftströmungen in Gebäuden", Zurich, Switzerland, 1989 (French and German).
- 4. J.-L. Scartezzini, J.-M. Fürbringer, C.-A. Roulet
 "Data needs for purpose of air infiltration computer code validation"
 8th AIVC Conference proceedings, Ueberlingen, RFA, 1987.
- 5. J.-M. Fürbringer, C. Roecker, C.-A. Roulet
 "The use of a guarded zone pressurization technique to measure air
 flow permeabilities of a multi-zone building"

 9th AIVC Conference proceedings, Gent, Belgium, 1988.
- 6. J.-M. Fürbringer, R. Compagnon, C.-A. Roulet, A. Gadilhe "Wind and pressure requirements of the validation of a multi-zone air infiltration program"

 10th AIVC Conference proceedings, Espoo, Finland, 1989.
- 7. J.-M. Fürbringer, C.-A. Roulet
 "Study of the errors occurring in measurement of leakage distribution in buildings by multifan pressurisation"

 Submitted to "Building and Environment", Feb. 1990.
- 8. J.-M. Fürbringer, R. Compagnon
 "Weather and aeraulic data-set for validation: the LESO building"
 Part I: "Content of the data-set" LESO Internal report (1989).
- 9. A. Faist et al. Projet NEFF 110 "Rapport de Synthèse" LESO report, Lausanne, Switzerland, 1985.
- Institut Suisse de Météorologie "Valeurs journalières des précipitations enregistrées aux stations météorologiques et pluviométriques suisses" ISM, Zurich (4ème trimestre 1988).

2. TEST SITE DESCRIPTION

2. TEST SITE DESCRIPTION

2.1 Geographic information

1.1.1 Location

The LESO building is a laboratory building of the Ecole Polytechnique Fédérale, which is in Ecublens near Lausanne, a suburban area, at 500 [m] of the lake shore.

Longitude:

E) 6.5

Latitude:

(N) - 46.53

2.1.2 Height above the sea level

The front door is at ≈ 400 m above the sea level.

2.1.3 Terrain

Suburban area. The building is surrounded by slightly higher buildings (see Annex 3).

2.1.4 Orientation

The building has its main axis East-West, the main façade, mostly glazed, is south oriented.

2.15 Location of meteorological station

The building has its own meteorological station. Temperatures, reference pressure, air moisture, solar radiation are measured on the roof of the building.

The wind speed and direction are measured at 18.2 [m] from ground level, on a mast 5.5 [m] over the roof. Figure 2.2 presents the location of the probes on the building.

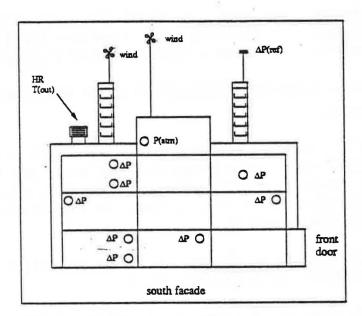


Figure 2.2: South façade of the LESO Building with meteorological parameters probes position.

2.2 Climatic information

2.2.1 Distribution of wind speed versus direction

Two kinds of distributions are presented to evaluate the wind speed versus direction distribution from quarterly wind speed and direction measurements:

- The wind occurrence percentage in a given sector which indicates the orientation distribution without intensity information.
- The average wind integral (relative or not) in a given sector which indicates the distribution of the wind intensity.

The statistics and the graphics are extracted from 1989 all year measurements and from the two tracer gas measurement periods included in the data-set.

Figure 2.3 presents the distribution of the wind direction in 1989 in 36 sectors of 10° (south = 0° , West = 90° , North = 180°). The dominant winds come from North and South. This corresponds to the main winds in the area (north and south-west), the effect being enhanced by the surrounding buildings.

The average wind speed, calculated for every month in 1989 is presented in figure 2.4. The mean value is between 2 and 3 [m/s]. These winds are however feeble when compared to coastal areas or flat countries.

To have a statistical signification, this data should concern a longer time (= 10 years).

Figure 2.5 presents the relative wind integral for a 10 days period in December 1987 which corresponds with the tracer gas measurements. During this period the average wind speed has been west (m/s) with a dominant direction. The relative occurrences distribution presented in figure 2.6 confirms this results.

The same statistics for the year 1988 measurement period (figures 2.7 and 2.8) have given a dominant north wind.

Table 2.1 presents daily averages of wind speed, external temperature and moisture, insolation for the periods which correspond with the tracer gas measurement campaigns.

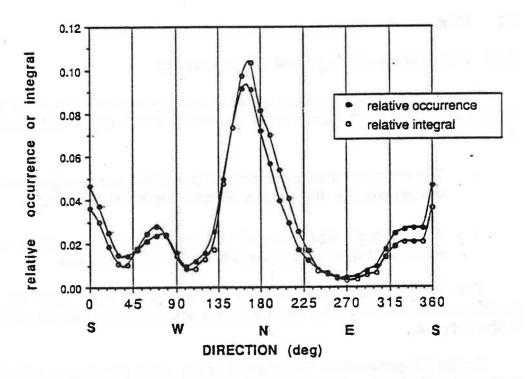


Figure 2.3: Wind relative distribution (occurrences and integral) in 1989 from quartely wind measurement on the LESO-building.

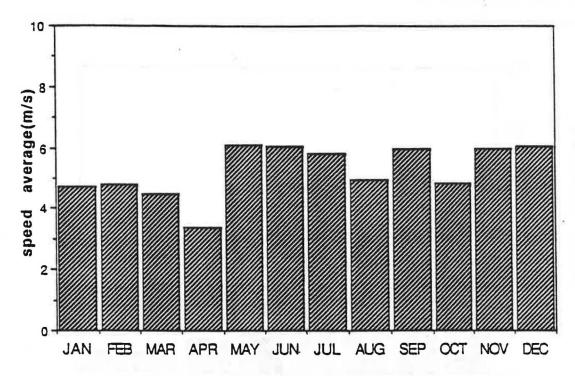


Figure 2.4: Monthly average wind speed in 1989 from quartely wind measurement on the LESO-building.

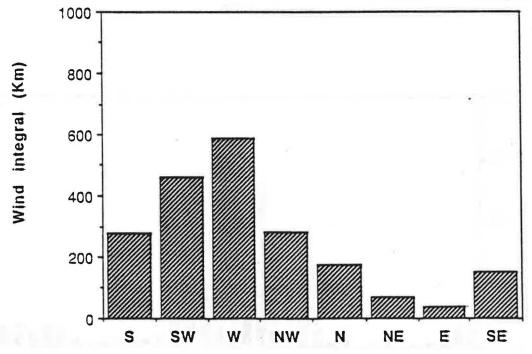


Figure 2.5: Wind integral distribution for the 10 days measurement period in 1987.

2. TEST SITE DESCRIPTION

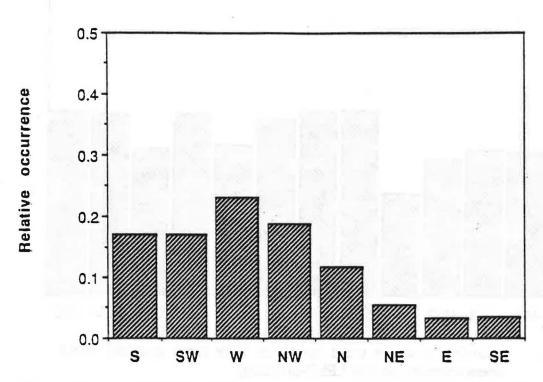


Figure 2.6: Relative wind occurrence distribution for the 10 days measurement period in 1987.

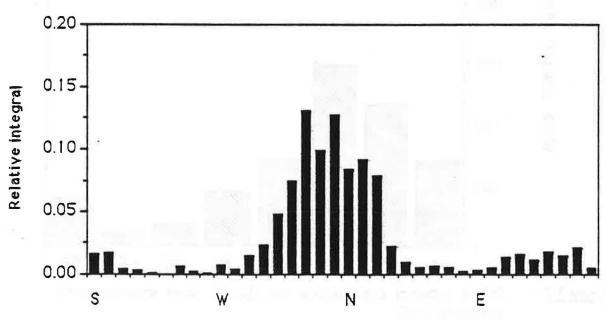


Figure 2.7: Wind integral relative distribution for the measurement period B in 1988.

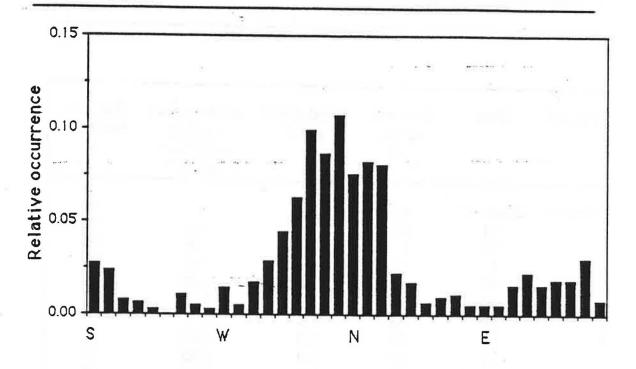


Figure 2.8: Relative wind occurrence distribution for the measurement period B in 1988.

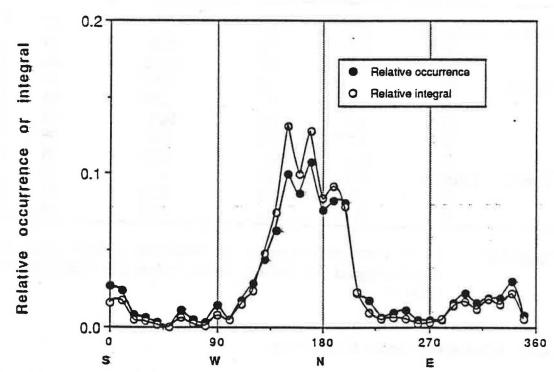


Figure 2.9: Relative wind occurrence and integral comparison for the measurement period B in 1988.

2. TEST SITE DESCRIPTION

| Period | Date | Date External temp. | | South global vertical insolation [MJ/m ²] | Relative humidity % |
|---------|------------|---------------------|-----|--|---------------------------|
| 1987 A | 23 déc. 87 | 4.2 | 1.8 | _ | 81 |
| 1707 11 | 24 | 3.1 | 1.6 | 1.03 | 85 |
| | 25 | 4 | 1.3 | .99 | 91 |
| | 26 | 5.4 | 1.6 | 1.24 | 88 |
| | 27 | 4.5 | 1.4 | 1.36 | 91 |
| | 28 | 3.8 | 1.4 | 1.40 | 93 |
| | 29 | 2.8 | 1.3 | 1.10 | 92 |
| | 30 | 2.8 | 1.3 | 4.85 | 91 |
| | 31 | 3.7 | 1.0 | 2.23 | 89 |
| | 1 jan. 88 | 6.1 | 1.5 | 1.10 | 88 |
| | 2 | 8.1 | 3.5 | 6.09 | <i>7</i> 9 |
| | 3 | 7.6 | 4.3 | 5.48 | 77 |
| | 4 | 4.8 | 5.1 | 0.46 | 87 |
| 1988 A | 24 déc. 88 | 8.2 | 2.3 | _ | 77 |
| | 25 | 7.7 | 1.3 | 36.8 | 84 |
| | 26 | 4.5 | 1.8 | 50.45 | 86 |
| 1988 B | 27 | 5 | .8 | 2.97 | 89 |
| | 28 | 4.4 | 2 | 1.79 | 84 |
| | 29 | 1.5 | 2.9 | 44.9 | 92 |
| | 30 | 2.7 | 1.1 | 5.31 | 89 |
| | 31 | 0.8 | 2 | 2.75 | 93 |
| 1988 C | 2 jan. 89 | -0.2 | 3.9 | • | 84 |
| | 3 | 0 | 2.3 | 2.26 | 81 |
| | 4 | -1.I | 3.0 | 2.25 | 86- |

<u>Table 2.1</u>: Daily averages (excepted for insolation : daily sum) of meteorological parameters during tracer gas measurement periods.

2.2.2 Wind speed versus temperature

- This information can be obtained from the full data-set, but is not shown here.

2.2.3 Solar radiation

Table 2.2 gives the list of the insolation measurements included in the data-set, since table 2.1 has exibited the daily averaged insolation during the tracer gas measurement periods.

| Par | rameter | Chann | Unit | |
|---------|------------|---------|------|------------------|
| Global | Horizontal | can 102 | SM | W/m ² |
| Diffuse | Horizontal | can 124 | SM | W/m^2 |
| Global | South | can 106 | SM | W/m ² |

<u>Table 2.2</u>: Insolation parameters included in the data-set.

Figures 2.10 - 2.12 present three years of monthly averaged insolation and outside air temperature.

2.2.4 Cloudiness

No information available.

2.2.5 Precipitation, humidity

No information on precipitation is contained in the set.

The Swiss meteorology institute gives for the region of Lausanne in 1988, 1249 [mm] of precipitation since the annual average between 1901 and 1960 is 1064 [mm] of water [10].

2. TEST SITE DESCRIPTION

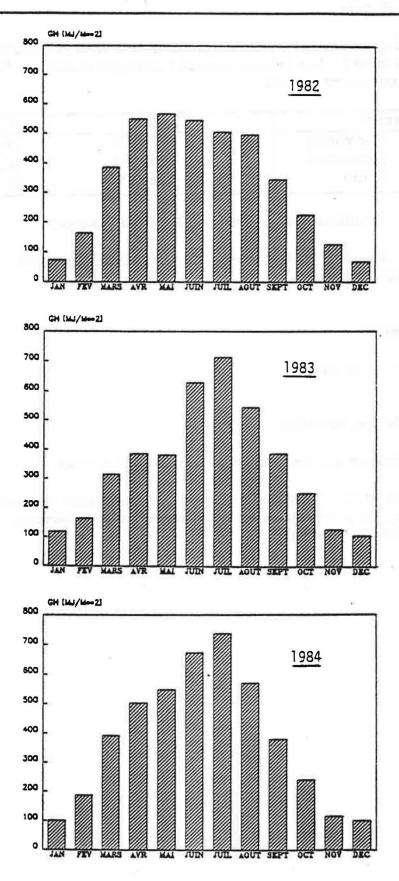


Figure 2.10: Global horizontal insolation measured in the LESO.

さら、一方言語の経済第一、一方は日本の大大大学

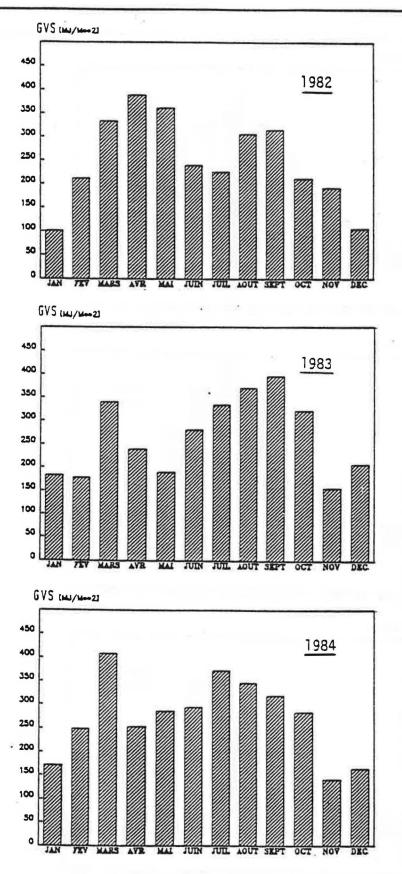


Figure 2.11: Global vertical insolation measured in the LESO.

2. TEST SITE DESCRIPTION

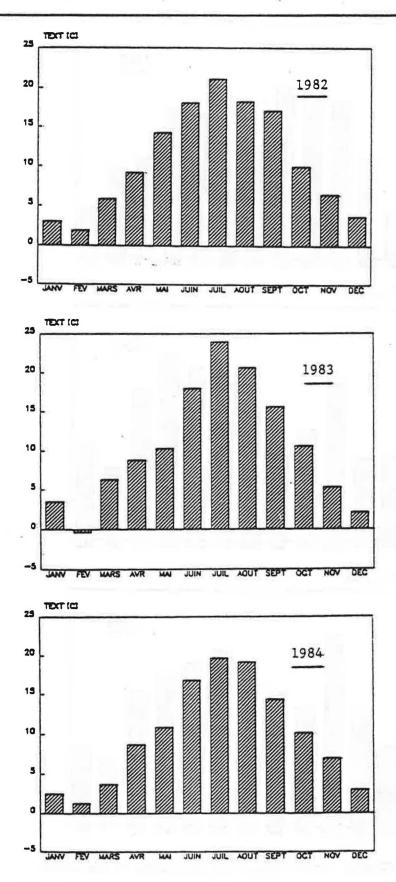


Figure 2.12: Monthly averaged outside air temperature.

3.1 Building name LESO (Laboratoire d'Energie Solaire)

3.2 Building type Administrative, office building

3.3 History

The LESO-building was built in 1983 to serve as laboratory and work office to the LESO-PB (Laboratory of solar energy and building physics) [9].

After few years of study on the thermal problems attached to the passiv solar systems, the laboratory has now expanded in domain to energy in buildings and a group is specialised on air infiltration research.

3.4 Construction

The building is constituted of nine south oriented cells with different façades and 10 [cm] insulation between the cells themselves.

The thermal insulation is very high: 20 [cm] between inside and outside. The structure is in concrete. The partition walls are non finished concrete blocs.

Figures 3.1 - 3.4 present the thermal conductances.

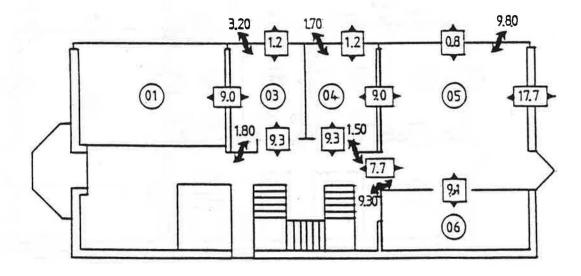


Figure 3.1: Thermal conductances in [W/K] between rooms and also with outside. First floor.

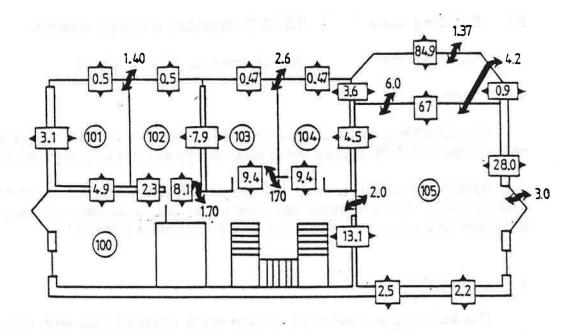


Figure 3.2: Thermal conductances in [W/K] between rooms and also with outside. Second floor.

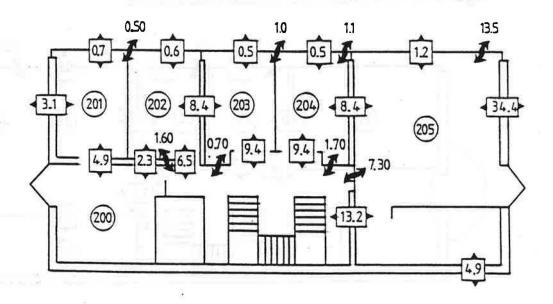


Figure 3.3: Thermal conductances in [W/K] between rooms and also with outside. Third floor.

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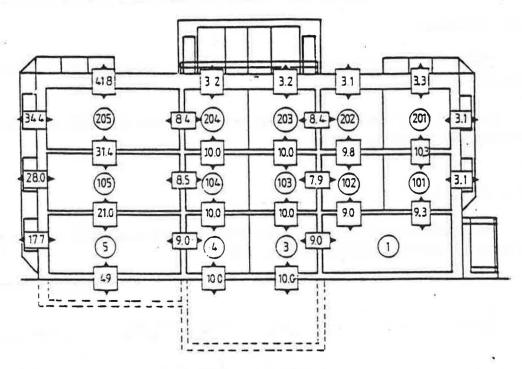


Figure 3.4: Thermal conductances in [W/K] between rooms and also with outside (South elevation). Circles contain room number.

3.5 Dimension

3.5.1 Plan see annex 3

3.5.2 Elevation see figure 3.12

3.5.3 Global parameters

| Total volume : Floor area : | | 2 165 785 | [m ³] [m ²] | |
|--------------------------------|--------------------------------|------------------------------|---|----|
| Window area: | South East North West | 118.3 5.5 - 2.1 2.7 | [m ²] [m ²] [m ²] | |
| K: | | .55 | $[W/m^2K]$ | |
| Total external area | .: | 833 | $[m^2]$ | ž. |
| Ground area: | | 346.5 | $[m^2]$ | |

3.5.4 Windows

There are various types of windows. A comprehensive description is given in reference [9].

In 1988 the greenhouse has been removed (room 005, 105) and now a conventional façade replaces it.

3.5.5 Front door

The front door is an air lock in metal framed glas, built untight for purpose of natural ventilation (see fig. 3.5).

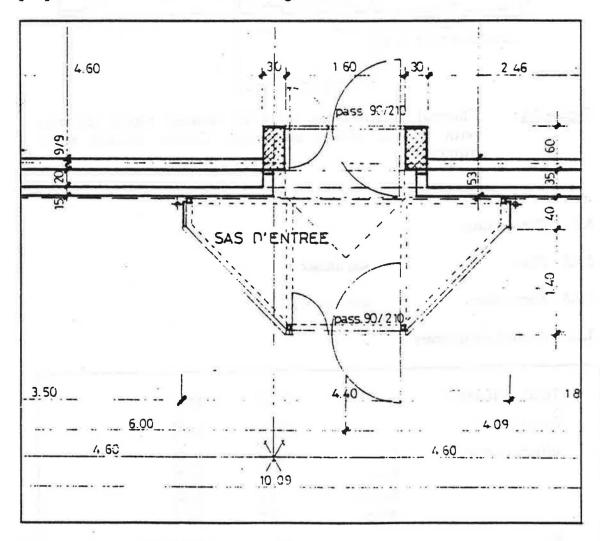


Figure 3.5: The front door plan.

3.5.6 Rooms

Figure 3.6 presents the plan of the rooms.

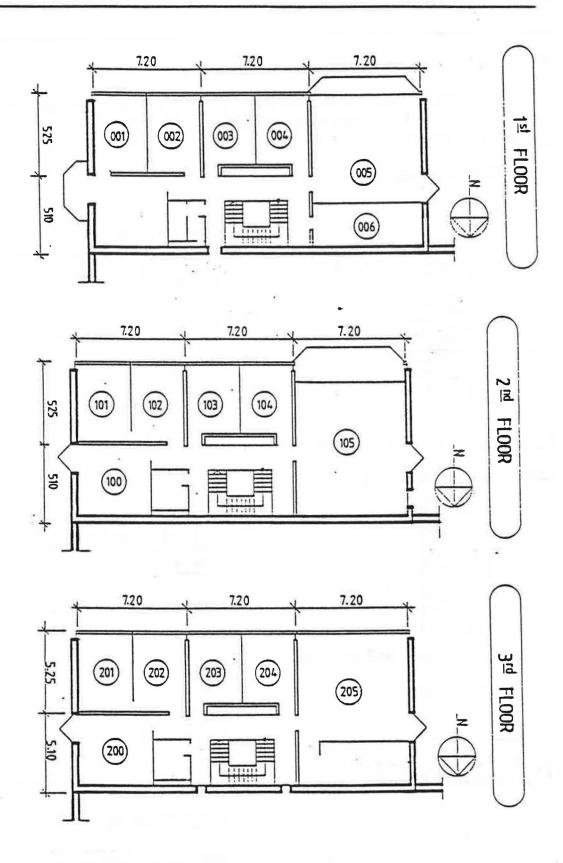


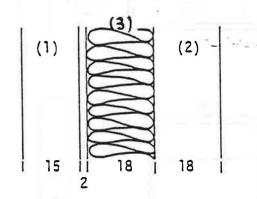
Figure 3.6: Plan of the rooms in the LESO building.

3.5.7 Roof

The roof is flat with the excrescence of the stair case and two chimneys (see fig. 2.2). It is a concrete dam with external, 20 [cm] thick insulation, covered with grave or concrete slabs.

3.5.8 Wall thickness

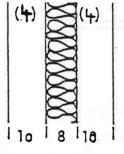
Outside walls



- (1) Concrete blocs $39.5 \times 19 \times 15 \text{ cm}^3 = 20.130 \text{ kg}$ 268 kg/m^2
- (2) Concrete blocs $39.5 \times 19 \times 18 \text{ cm}^3 = 22.333 \text{ kg}$ 298 kg/m^2
- (3) Glass wool $\lambda = 0.04 \text{ W/mK}$

Figure 3.7: Outside wall structure.

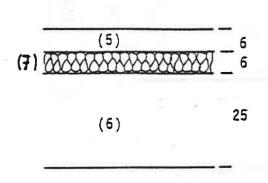
Lateral walls between cells



(4) Concrete blocs $49.5 \times 19 \times 10 \text{ cm}^3 = 12.357 \text{ kg}$ $\boxed{132 \text{ kg/m}^2}$

Figure 3.8: Inside wall structure.

Deck between floors



- (5) Covering (estimated)

 132 kg/m²
- (6) Sample ϕ 16 cm h = 32 cm weight 15.641 kg 2431 kg/m³ 608 kg/m^2
- (7) Glass wool $\lambda = 0.036 \text{ W/mK}$

Figure 3.9: Floor structure.

3.6 Air leakage information

The air leakage information consists on the values of the air conductances of the major elements of the building. The vertical air conductances have been neglected.

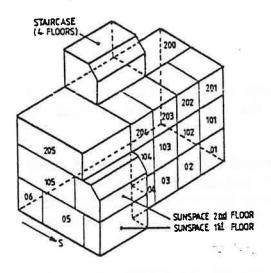
The measurement have been performed using the guarded zone technique. The technique is presented in [5] and discussion on the error is made in [7]. The authors want to emphasize on the necessity to consider this item as seriously as required since errors in leakage parameters could reach 100% in very common situations.

Figure 3.10 presents the aeraulic net of the LESO, the nodes corresponding to the rooms and the "resistances" to the air leakage.

Figure 3.11 presents the measurement results for C in $[m^3/h Pa^n]$ and for n since tables 3.1 - 4 give the list of the leakage like they are modelled for G.C. Comis code (C in $[kg/s Pa^n]$). This data concerns the building how it was in 1987.

The transformations made in the current of 1988 needed to perform additional measurement which will be included in the data as soon as possible (Summer 1990).

Some elements have not been separatly measured and have been estimated from global measurements as it is the case for the south and west façades of rooms 005, 105 and 205. Their own measurement would need a very complex experiment.



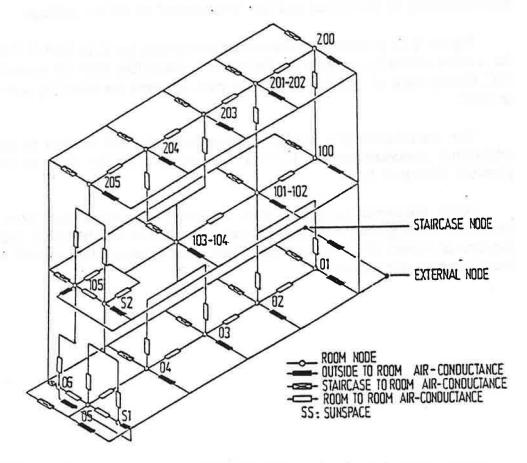


Figure 3.10: Perspective of the LESO-Building (top) and corresponding conductances net (bottom).

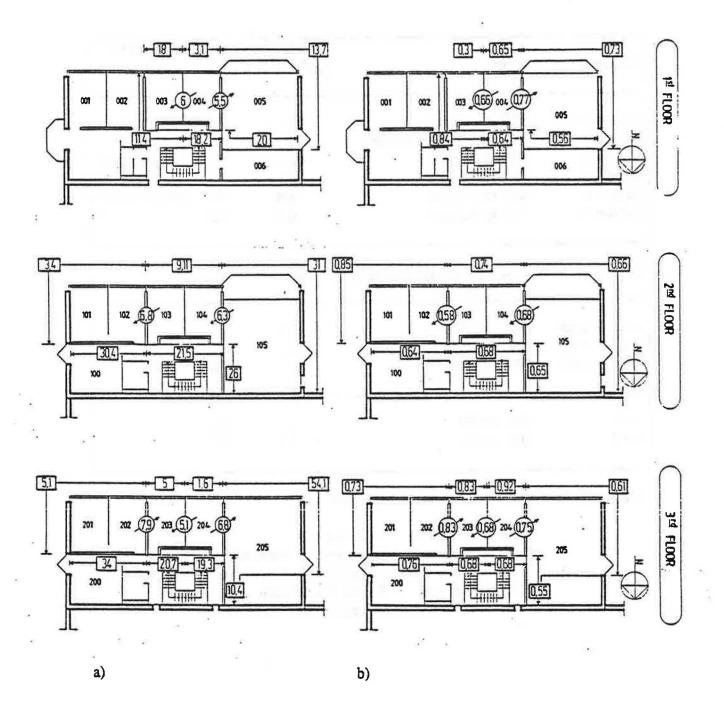


Figure 3.11: a) C-values of the LESO-Building C [m³/h Pan] b) Exponents n [-].

- values for exfiltration from a room to outside or staircase.
- Ø values for exfiltration from a room to another room with the sense of measurement.

| Element | from | C [m ³ /h Pa ⁿ] | n [-] | comments |
|-------------|--------------------------|---|----------|-------------|
| front door | STC to outside | 96 | .60 | |
| façade S | (001 and 002) to outside | 21 | .60 | |
| façade S | 003 to outside | 3.1 | .65 | estimated |
| façade S | 004 to outside | 3.1 | .65 | |
| façade S | 005 to outside | 6.8 | .73 | greenhouse* |
| façade W | 005 to outside | 6.8 | .73 | * |
| door N | STC to adjacent building | 20 | .60 | * |
| wall + door | 003 to STC | 11.4 | .84 | 1 4 1 |
| wall + door | 004 to STC | 18.2 | .64 | |
| wall + door | 005 to STC | 20 | .56 | |
| wall | 004 to 003 | 6 | .66 | |
| wall | 005 to 004 | 5.5 | .77 | |

Table 3.1: Air-conductances of the first floor of the LESO in 1987

STC means staircase

means that result is arbitrarily parted between different elements

S,E,N,W mean South, East, North and West

orientation of an element.

| Element | from | C [m ³ /h Pa ⁿ] | п [-] | comments | | |
|-------------|--------------------------|---|----------|-------------|--|--|
| façade E | 100 to outside | 15 | .6 | * | | |
| façade S | (101 and 102) to outside | 4 | .85 | | | |
| façade S | (103 and 104) to outside | 9.2 | .74 | | | |
| façade S | 105 to outside | 2.4 | .66 | *greenhouse | | |
| façade W | 105 to outside | 7.2 | .66 | * | | |
| window N | STC to outside | 15 | .6 | * | | |
| 11 . 1 | 101 1100 - 000 | 20.4 | | | | |
| wall + door | 101 and 102 to STC | 30.4 | .64 | | | |
| wall + door | 103 and 104 to STC | 21.5 | .68 | | | |
| wall + door | 105 to STC | 26 | .65 | | | |
| | 100 . 101 | 6.9 | .58 | | | |
| wall | 103 to 101 | 6.8 | 0 | | | |

Figure 3.2: Air-conductances of the second floor of the LESO in 1987

| SIC | means | staircase |
|---------|-------|------------------------------------|
| * | means | that result is arbitrarily |
| | | parted between different elements. |
| S,E,N,W | mean | South, East, North and West |
| | | orientation of an element. |

| Element | from | C [m ³ /h Pa ⁿ] | n [-] | comments |
|-------------|--------------------------|---|----------|---------------|
| window E | 200 to outside | 15 | .6 | * |
| façade S | (201 and 202) to outside | 5.1 | .73 | |
| façade S | 203 to outside | 1.6 | .83 | winter posit. |
| façade S | 204 to outside | 5 | .92 | summer pos. |
| façade S | 205 to outside | 9 | .61 | • |
| Façade W | 205 to outside | 7.2 | .61 | • |
| window N | STC to outside | 30 | .6 | |
| skylight | 200 to outside | 38.4 | .61 | vertical,* |
| skylight | 205 to outside | 38.4 | .61 | vertical,* |
| wall + door | 201 and 202 to STC | 34 | .76 | |
| wall + door | 203 to STC | 20.7 | .68 | |
| wall + door | 204 to STC | 19.3 | .68 | |
| wall + door | 205 to STC | 10.4 | .55 | |
| wall | 203 to 202 | 7.9 | .83 | |
| wall | 204 to 203 | 5.1 | .68 | |
| wall | 205 to 204 | 6.8 | .75 | |

Table 3.3:

Air-conductances of the third floor of the LESO in 1987.

STC means staircase

* means that result is arbitrarily parted between different elements

S,E,N,W mean South, East, North and West orientation of an element.

| Element | from | C [m ³ /h Pa ⁿ] | n [-] | comments |
|----------------------|----------------|---|----------|----------|
| window W | STC to outside | 5 | .6 | * |
| window S window + | STC to outside | 5 | .6 | * |
| door E | STC to outside | 10 | .6 | * |

Table 3.4: Air-conductance of the roof level of the LESO in 1987.

STC means staircase

* means that result is arbitrarily parted between different elements S,E,N,W mean South, East, North and West orientation of an element.

3.7 Pressure coefficients

Average pressure coefficients Cp have been measured by D. Dickeroff from LBL in the wind tunnel of the departement of Architecture in Berkeley University.

The measurement was made at a flow speed of 5 (m/s) on a 1:100 scale model.

The reference point for pressure and speed is settled at the top of the west chimney (fig. 2.2).

The wind profile simulated in the wind tunnel has an α = 0.152 \pm 0.09 according to the law

$$V = \left(\frac{h}{h_{ref}}\right)\alpha$$
 3.1

The measurement have been physically averaged through a tank of 100 (litres).

Figure 3.12 shows the elevations of the building with the probe positions and tables 3.5 - 8 present the pressures coefficients Cp for different angles of wind incidences.

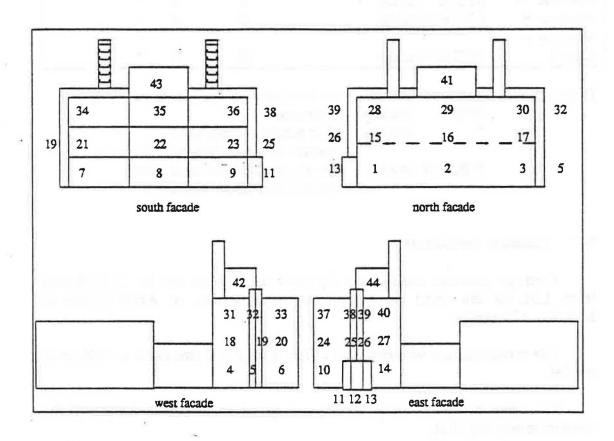


Figure 3.12: Elevations of the LESO-Building with the pressure tube positions (number).

| | , | | Pressure Co | efficients from | the LESO Mod | el | •_ | |
|-------|------|------|------------------|-----------------|--------------|------|------|---------|
| | | • | North W | all Measuremer | nt Positions | | | |
| Angle | 15 | 16 | 17 | 28 | 29 | 30 | 41 | average |
| 0 | 0.13 | 0.26 | 0.14 | 0.01 | 0.02 | 0.09 | 0.29 | 0.13 |
| 15 | 0.32 | 0.32 | 0.05 | 0.31 | 0.07 | 14 | 0.30 | 0.18 |
| 30 | 0.25 | 0.28 | 0.07 | 0.37 | 0.16 | 17 | 0.31 | 0.18 |
| 45 | 0.11 | 0.16 | 0.07 | 0.21 | 0.16 | 02 | 0.13 | 0.12 |
| 60 | 0.00 | 0.04 | 0.06 | 0.07 | 0.04 | 0.03 | 07 | 0.02 |
| 75 | 23 | 04 | 0.04 | 14 | 05 | 0.01 | 16 | 08 |
| 90 | 44 | 15 | - .04 | 40 | 15 | 06 | 25 | 21 |
| 105 | 40 | 16 | 07 | 40 | 21 | 09 | 31 | 24 |
| 120 | 12 | 07 | 04 | 21 | 15 | 06 | 29 | 13 |
| 135 | 08 | 04 | 04 | 31 | 20 | 09 | 25 | 14 |
| 150 | 05 | 07 | 11 | 26 | 19 | 12 | 22 | 15 |
| 165 | 18 | 13 | 13 | 28 | 22 | 14 | 24 | 19 |
| 180 | 16 | 13 | 14 | 19 | 17 | 18 | 17 | 16 |
| 195 | 15 | 15 | 20 | 16 | 23 | 28 | 24 | 20 |
| 210 | 06 | 05 | 08 | 09 | 18 | 25 | 20 | 13 |
| 225 | 01 | 01 | 09 | 04 | 13 | 21 | 14 | 09 |
| 240 | 0.15 | 0.11 | 0.10 | 0.14 | 0.05 | 01 | 02 | 0.07 |
| 255 | 0.05 | 0.03 | 0.09 | 0.02 | 07 | 05 | 11 | 00 |
| 270 | 04 | 02 | 0.11 | 05 | 06 | 0.03 | 18 | 03 |
| 285 | 01 | 0.03 | 0.14 | 03 | 0.01 | 0.14 | 04 | 0.03 |
| 300 | 01 | 0.01 | 0.01 | 03 | 0.01 | 0.09 | 0.04 | 0.02 |
| 315 | 0.08 | 0.09 | 04 | 04 | 0.06 | 0.10 | 0.18 | 0.06 |
| 330 | 0.08 | 0.16 | 05 | 16 | 0.06 | 0.09 | 0.30 | 0.07 |
| 345 | 0.04 | 0.26 | 0.04 | 20 | 0.02 | 0.14 | 0.35 | 0.09 |
| 360 | 0.13 | 0.25 | 0.11 | 0.00 | 0.01 | 0.05 | 0.37 | 0.13 |

Table 3.5: North façade mean pressure coefficients Cp for different wind incidences, 0° corresponding to North and 90° corresponding to East wind incidence. The probe position are shown in figure 3.12.

| | | | | | Pres | sure Co | efficient | from t | he LESC | Model (| 16 | | | | |
|-------|------|------|------|------|------|---------|-----------|---------|----------|---------|------|------|------|------|---------|
| | | | | | | East Wa | II Meas | irement | Position | ns | | | | | |
| Angle | 10 | - 11 | 12 | 13 | 14 | 24 | 25 | 26 | 27 | 37 | 38 | 39 | 40 | 44 | average |
| 0 | 12 | 19 | 13 | 0.08 | 0.07 | 11 | 26 | 0.05 | 0.00 | 16 | 27 | 0.06 | 02 | 19 | 08 |
| 15 | 18 | 30 | 22 | 0.22 | 0.31 | 22 | 33 | 0.35 | 0.31 | 21 | 40 | 0.46 | 0.27 | 03 | 0.00 |
| 30 | 17 | 24 | 23 | 0.33 | 0.44 | 12 | 25 | 0.44 | 0.42 | 0.01 | 34 | 0.53 | 0.42 | 0.01 | 0.09 |
| 45 | 0.01 | 06 | 06 | 0.41 | 0.49 | 0.16 | 08 | 0.52 | 0.51 | 0.34 | 14 | 0.62 | 0.56 | 0.07 | 0.24 |
| 60 | 0.21 | 0.14 | 0.19 | 0.48 | 0.54 | 0.39 | 0.16 | 0.63 | 0.62 | 0.52 | 0.13 | 0.69 | 0.67 | 0.22 | 0.40 |
| 75 | 0.39 | 0.36 | 0.39 | 0.55 | 0.57 | 0.55 | 0.48 | 0.69 | 0.65 | 0.60 | 0.43 | 0.71 | 0.68 | 0.40 | 0.53 |
| 90 | 0.55 | 0.50 | 0.53 | 0.61 | 0.62 | 0.62 | 0.67 | 0.72 | 0.68 | 0.71 | 0.68 | 0.75 | 0.65 | 0.21 | 0.61 |
| 105 | 0.52 | 0.50 | 0.54 | 0.54 | 0.57 | 0.58 | 0.68 | 0.65 | 0.60 | 0.70 | 0.70 | 0.68 | 0.63 | 0.33 | 0.59 |
| 120 | 0.14 | 0.13 | 0.17 | 0.19 | 0.25 | 0.14 | 0.19 | 0.20 | 0.19 | 0.22 | 0.21 | 0.19 | 0.21 | 0.25 | 0.19 |
| 135 | 0.06 | 0.07 | 0.02 | 0.04 | 0.05 | 0.01 | 0.12 | 05 | 00 | 0.10 | 0.17 | 10 | 0.02 | 0.22 | 0.05 |
| 150 | 23 | 22 | 16 | 09 | 06 | 28 | 17 | 18 | 14 | 30 | 16 | 25 | 19 | 0.01 | 17 |
| 165 | 19 | 06 | 13 | 07 | 08 | 25 | 04 | 29 | 17 | 18 | 10 | 34 | 28 | 03 | 16 |
| 180 | 26 | 20 | 19 | 13 | 12 | 28 | 19 | 23 | 20 | 27 | 23 | 26 | 24 | 16 | 21 |
| 195 | 34 | 27 | 23 | 19 | 18 | 35 | 29 | 22 | 21 | 35 | 33 | 22 | 22 | 25 | 26 |
| 210 | 47 | 23 | 24 | 16 | 13 | 49 | 37 | 20 | 20 | 40 | 37 | 20 | 22 | 22 | 28 |
| 225 | 32 | 01 | 18 | 08 | 08 | 34 | 15 | 13 | 09 | 25 | 18 | 11 | 09 | 15 | 15 |
| 240 | 01 | 0.22 | ~.05 | 0.08 | 0.08 | 18 | 0.11 | 0.02 | 0.02 | 10 | 01 | .01 | 0.00 | 06 | 0.01 |
| 255 | 02 | 0.08 | 02 | 0.01 | 0.02 | 06 | 0.06 | 0.02 | 0.02 | 05 | 0.00 | 0.02 | 0.03 | 05 | 0.00 |
| 270 | 14 | 12 | 10 | 09 | 08 | 14 | 13 | 11 | 12 | 13 | 14 | 11 | 10 | 16 | 12 |
| 285 | 14 | 13 | 10 | 08 | 07 | 15 | 14 | 11 | 11 | 16 | 16 | 13 | 12 | 21 | 13 |
| 300 | 16 | 14 | 12 | 11 | 10 | 16 | 14 | 13 | 11 | 18 | 15 | 14 | 13 | 28 | 15 |
| 315 | 11 | 10 | 10 | 07 | 07 | 11 | 10 | 09 | 10 | 12 | 12 | 11 | 11 | 28 | 11 |
| 330 | 10 | 12 | 17 | 17 | 16 | 14 | 13 | 19 | 21 | 14 | 13 | 19 | 18 | 27 | 16 |
| 345 | 13 | 15 | 13 | 12 | 09 | ₹.14 | 19 | 13 | 23 | 15 | 19 | 17 | 20 | 31 | 17 |
| 360 | 14 | 18 | 14 | 0.06 | 0.07 | 13 | 29 | 0.01 | 04 | 19 | 29 | 0.03 | 06 | 22 | 11 |

Table 3.6: East façade mean pressure coefficients Cp for different wind incidences, 0° corresponding to North and 90° corresponding to East wind incidence. The probe position are shown in figure 3.12.

| | | | | South | Wall Meas | urement P | ositions | | | | ĺ |
|-------|------|------|------|-------|-------------|-----------|----------|------|------|------|---------|
| Angle | 7 | 8 | 9 | 21 | 22 | 23 | 34 | 35 | 36 | 43 | average |
| O | 10 | 11 | 11 | 09 | 10 | 11 | 10 | 11 | 12 | 25 | -,12 |
| 15 | 09 | -,10 | 10 | 09 | 08 | 10 | 10 | 09 | 09 | 26 | -,11 |
| 30 | 12 | 10 | 10 | 12 | 10 | 10 | 11 | 11 | 11 | 27 | 12 |
| 45 | 14 | 12 | 11 | 16 | 12 | 13 | 14 | 13 | 12 | 30 | 15 |
| 60 | 18 | 22 | 18 | 21 | √ 25 | 18 | 19 | 23 | 22 | 34 | 22 |
| 75 | 13 | 29 | 21 | 21 | 30 | 24 | 25 | 29 | 22 | 35 | 25 |
| 90 | 0.01 | 13 | 34 | 01 | 17 | 41 | 05 | 19 | 35 | 22 | 19 |
| 105 | 0.14 | 0.11 | 06 | 0.11 | 0.10 | 18 | 0.09 | 0.09 | 07 | 0.03 | 0.04 |
| 120 | 0.27 | 0.18 | 0.14 | 0.23 | 0.20 | 0.07 | 0.17 | 0.19 | 0.17 | 0.14 | 0.18 |
| 135 | 0.36 | 0.32 | 0.25 | 0.39 | 0.38 | 0.30 | 0.35 | 0.36 | 0.32 | 0.19 | 0.32 |
| 150 | 0.74 | 0.65 | 0.40 | 0.84 | 0.76 | 0.53 | 0.69 | 0.61 | 0.50 | 0.06 | 0.58 |
| 165 | 0.43 | 0.55 | 0.46 | 0.50 | 0.62 | 0.55 | 0.56 | 0.63 | 0.67 | 0.36 | 0.53 |
| 180 | 0.49 | 0.53 | 0.36 | 0.58 | 0.59 | 0.43 | 0.60 | 0.60 | 0.53 | 0.15 | 0.48 |
| 195 | 0.48 | 0.51 | 0.38 | 0.53 | 0.57 | 0.48 | 0.59 | 0.59 | 0.53 | 0.17 | 0.48 |
| 210 | 0.48 | 0.65 | 0.75 | 0.62 | 0.82 | 0.88 | 0.61 | 0.62 | 0.75 | 03 | 0.61 |
| 225 | 0.24 | 0.37 | 0.54 | 0.34 | 0.44 | 0.49 | 0.28 | 0.28 | 0.32 | 01 | 0.33 |
| 240 | 0.26 | 0.30 | 0.60 | 0.23 | 0.35 | 0.42 | 0.28 | 0.27 | 0.33 | 0.28 | 0.33 |
| 255 | 0.03 | 0.08 | 0.17 | 0.02 | 0.07 | 0.11 | 0.03 | 0.04 | 0.06 | 00 | 0.06 |
| 270 | 14 | 01 | 0.01 | 19 | 05 | 02 | 21 | 11 | 07 | 24 | 10 |
| 285 | 38 | 0.06 | 0.03 | 42 | 18 | 05 | 34 | 22 | 14 | 41 | 20 |
| 300 | 40 | 0.00 | 01 | 47 | 18 | 04 | 36 | 25 | 14 | 35 | 22 |
| 315 | 34 | 18 | 15 | 33 | 21 | 14 | 31 | 22 | 15 | 32 | 24 |
| 330 | 09 | 10 | 10 | 09 | 08 | 10 | 09 | 07 | 10 | 20 | 10 |
| 345 | 11 | 12 | 13 | 10 | 11 | 13 | 10 | 10 | 12 | 26 | 13 |
| 360 | 12 | 12 | 12 | 10 | 11 | 13 | 11 | 11 | 13 | 26 | 13 |

Table 3.7: South façade mean pressure coefficients Cp for different wind incidences, 0° corresponding to North and 90° corresponding to East wind incidence. The probe position are shown in figure 3.12.

| | | | | | | | LESO Mod | el | | | |
|-------|------|------|--------|------|-----------|------|----------|------|------|------|---------|
| | } | | | West | Wall Meas | | | | | | |
| Angle | 4 | 5 | 6 | 18 | 19 | 20 | 31 | 32 | 33 | 42 | average |
| 0 | 0.12 | 0.22 | 26 | 0.13 | 23 | 26 | 0.07 | 0.16 | 28 | 10 | 04 |
| 15 | 05 | 0.09 | 20 | 26 | 23 | 21 | 25 | 24 | 19 | 27 | -,18 |
| 30 | 0.01 | 0.12 | 03 | 33 | 26 | 18 | 37 | 33 | 18 | 29 | 18 |
| 45 | 0.12 | 0.19 | 0.10 | 25 | 22 | 09 | 36 | 34 | 12 | 26 | 12 |
| 60 | 0.08 | 0.09 | 0.04 | 07 | 08 | 04 | 12 | 16 | 05 | 20 | 05 |
| 75 | 02 | 07 | 0.02 | 03 | 00 | 09 | 04 | 07 | 14 | 19 | 06 |
| 90 | 04 | 12 | 07 | 09 | 07 | 13 | 08 | 11 | 14 | 15 | 10 |
| 105 | 06 | 11 | 17 | 10 | 16 | 17 | 11 | 15 | 18 | 21 | 14 |
| 120 | 08 | 10 | T -,13 | 10 | 02 | 20 | 07 | 11 | 19 | 19 | 12 |
| 135 | 11 | 14 | 22 | 12 | 07 | 28 | 11 | 12 | 25 | 23 | 16 |
| 150 | 26 | 26 | 51 | 25 | 25 | 55 | 22 | 24 | 51 | 25 | 33 |
| 165 | 19 | 22 | 30 | 20 | 19 | 36 | 20 | 22 | 35 | 26 | 25 |
| 180 | 26 | 30 | 25 | 17 | -,03 | 32 | 29 | 33 | 30 | 13 | 24 |
| 195 | 18 | 29 | 23 | 29 | 06 | 29 | 33 | 39 | 23 | 05 | 23 |
| 210 | 05 | 09 | +.22 | 11 | 22 | 32 | 13 | 24 | 34 | 01 | 17 |
| 225 | 03 | 09 | 11 | 09 | 06 | 16 | 07 | 19 | 10 | 0.12 | 08 |
| 240 | 0.23 | 0.33 | 0.19 | 0.19 | 0.21 | 0.18 | 0.22 | 0.11 | 0.22 | 0.28 | 0.21 |
| 255 | 0.27 | 0.33 | 0.08 | 0.18 | 01 | 0.02 | 0.25 | 0.23 | 0.13 | 0.30 | 0.18 |
| 270 | 0.36 | 0.33 | 0.14 | 0.27 | 09 | 02 | 0.51 | 0.49 | 0.31 | 0.53 | 0.28 |
| 285 | 0.43 | 0.44 | 0.19 | 0.43 | 08 | 0.08 | 0.62 | 0.66 | 0.42 | 0.70 | 0.39 |
| 300 | 0.41 | 0.45 | 0.09 | 0.44 | 07 | 0.14 | 0.52 | 0.56 | 0.43 | 0.42 | 0.34 |
| 315 | 0.33 | 0.45 | 18 | 0.35 | 24 | 04 | 0.34 | 0.40 | 0.14 | 0.08 | 0.16 |
| 330 | 0.23 | 0.38 | 28 | 0.27 | 30 | 31 | 0.30 | 0.40 | 22 | 0.01 | 0.05 |
| 345 | 0.18 | 0.33 | 30 | 0.26 | 26 | 31 | 0.28 | 0.40 | 32 | 05 | 0.02 |
| 360 | 0.09 | 0.23 | 25 | 0.02 | 24 | 26 | 0.05 | 0.19 | 27 | 12 | 06 |

West façade mean pressure coefficients Cp for different wind incidences, 0° corresponding to North and 90° corresponding to East wind incidence. The probe position are shown in figure 3.12. Table 3.8:

4. OPERATION AND NUMERICAL DATA SET

4.1 Tracer gas campaigns

During the tracer gas measurement periods the building is not inhabited. The ventilation is off, the windows are closed and the inside doors are opened or closed depending on the experimental plans presented in figures 4.1 - 2 and table 4.1. The heating system is controlled at 19 [°C] with a PID controller in each room.

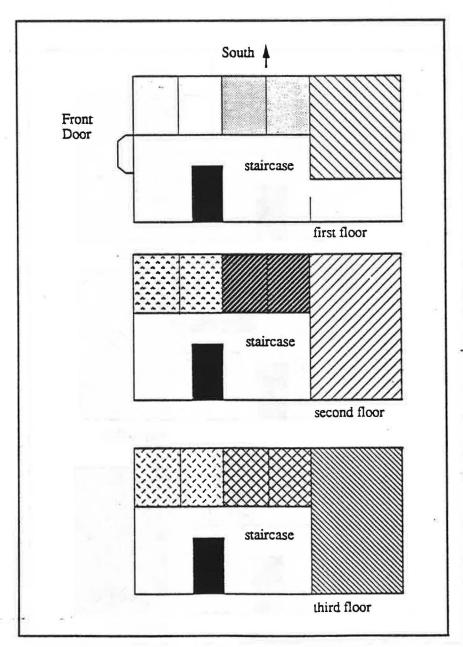


Figure 4.1: Experimental plan for tracer gas measurement in December 87. The dashed surfaces represent the measured rooms.

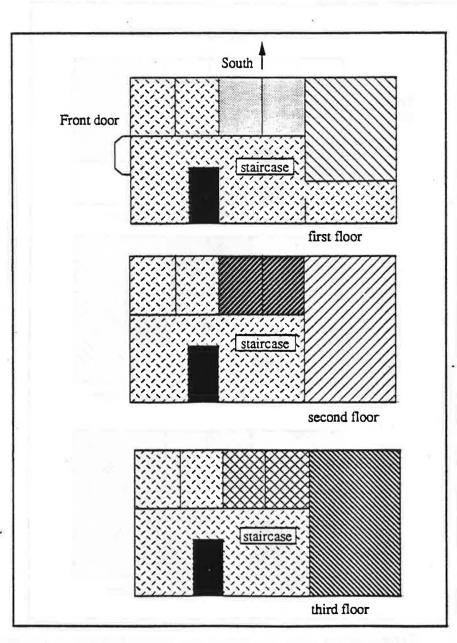


Figure 4.2: Experimental plan for tracer gas measurement in December 88. The dashed surfaces represent the measured rooms. In 1988 N₂O has been also injected in the staircase.

| Room | to | floor | Door 1987 | position 1988 |
|---|--|-------|--|--|
| 001 | hall hall hall hall hall hall | 1 | open | open |
| 002 | | 1 | open | open |
| 003 | | 1 | closed | closed |
| 004 | | 1 | closed | closed |
| 005 | | 1 | closed | closed |
| 006 | | 1 | open | open |
| 100 101 102 103 103 104 105 | 101 102 102 hall 103 hall 103 104 104 hall | | open open closed closed open closed closed | open open open closed closed closed closed |
| 200 | hall | 3 | open | open |
| 201 | 202 | 3 | open | open |
| 202 | hall | 3 | closed | open |
| 203 | hall | 3 | closed | closed |
| 204 | hall | 3 | closed | closed |
| 205 | hall | 3 | closed | closed |

<u>Table 4.1</u>: Position of the doors during the tracer gas measurement campains.

4.2 Available numerical data files

4.2.1 Nomenclature

No. of the last of

All data files concerning tracer gas measurements of air renewals and corresponding weather data are identified as follows:

LESOaa Axxx.yyy

with the meaning:

LESO measurements performed in purpose of validation of air infiltration codes

aa year of measurement (beginning)

A identification of the series of measurements. A serie being a continue following of measurements with a constant time step (1988 data has three periods A.B.C.)

xxx identification of the content (see later)

yyy format identification. The available files are written in our own data format, called GRES (Annex 1) identified by yyy = DAT.

4.2.2 Different files

The 1987-measurement files include measurement data collected between day 357 at 19h.15 (December 23rd, 1987) until day 369 at 14h.30 (January 4th, 1988).

The 1988 measurement files include three periods:

A, from day 358 at 21h.20 (December 24th 1987) to day 360 at 15h.40)

B, from day 360 at 18h.20 to day 365 at 24h.)

C, from day 367 at 19h. to day 369 at 14h. (January 4th 1989)

Measurements have been performed quarterly but the data files are available with a time step of 15 minutes or 30 minutes (version "30").

- Files LESOaaAVNR.DAT contain the weather data and building data (the comprehensive list is given in Annex 2)
 - Meteorological data
 - Room temperatures
 - Indoor-outdoor temperatures
 - Electrical consumption.
- Files LESOaaAREN.DAT contain the air flows Q_{Ai} incoming in each measured room (unity: [m³/s]) and also the confidence intervals (cf. Annex 2).
- Files LESOaaANJI.DAT contain the η_{ji} coefficients of equation 4.1 describing the air flows between the room i and the staircase and also the adjacent rooms j

$$Q_{Ai} = Q_{oi} + \sum_{j=1}^{N} \eta_{ji} Q_{ji}$$
 4.1

QAi: measured air flow in room i

Qoi : resultant air flow between the room and outdoor

Qii : resultant air flow between the rooms i and j

• Files LESOaaATEM.DAT give the mean temperature (high = 1.4 [m]) and the gradient between 0.5 [m] and 2.3 [m] for each room (unity [°C]).

4.2.3 Channel codification

The LESO-PB performing meteorological measurements since a few years, has developed his own standard codification to spot the different kinds of measurements in the records.

This codification is constituted by two letters (X, Y). The first (X) gives information on the *physical quantity*. The second (Y) precises the *type of record*: the data logger scans the channels at short time intervals (*measuring intervals*) and records the data at longer intervals (*recording interval*). It has then the possibility to record on the tape for every recording interval either the *instantaneous value* or the *integrated value* which is the sum of the measurements performed during the recording intervals or the *average value* which is the integrated value divided by the measurements number. Table 4.2 gives the code for X and Y:

| 1 | X : | P | \rightarrow | Temperature (Pt100) |
|-----|------------|----|---------------|--|
| | | E | \rightarrow | Power (or Energy if integrated) |
| | | K | \rightarrow | Pressure . |
| | | S | \rightarrow | Solar radiation |
| | | G. | \rightarrow | Opening angle (window, doors) |
| | | D | \rightarrow | Wind direction |
| | | W | \rightarrow | Wind speed |
| | | V | \rightarrow | Wind projection (sin, cos) |
| | | H | \rightarrow | Humidity |
| | | F | \rightarrow | Flow |
| | | | | |
| | Υ: | N | \rightarrow | Instantaneous value |
| | | M | \rightarrow | Averaged value during the recording interval |
| | | I | \rightarrow | Integrated (sum) value during the recording interval |
| | | S | \rightarrow | Root mean square during the recording interval |
| - 1 | | | | |

Table 4.2: Channel codification in the LESO data set.

4.2.4 Channel list

Annex 2 gives the list of the channels included in files described in paragraph 4.2.2 for 1987-data. 1988-data have some additional channels as a second static pressure probe (CSTB-probe) on channel 152 KM or the two ortogonal projections of the wind vector:

$$V_1 = |\overrightarrow{V}| \cos(\theta)$$

$$V_2 = |\overrightarrow{V}| \sin(\theta)$$
4.2
4.3

on channels 1 VM and 2 VM.

4.2.5 Defects on channels

The following channels have some defects in the file LESOaaAVNR.DAT:

C 451 KM, a differential pressure channel is defectuous from time 367/22:45 to 368/1:45 in 1987-data.

C 350 KM, a differential pressure channel is defectuous from time 363/4:45 to 364/12:00 in 1987-data.

C 21 PN is defectuous in all the data.

CONCLUSIONS

This document, together with the cited references, constitutes the first quoted draft of the description of the LESO validation data set.

It contains the description of numerous data measured on the LESO Building. Some of these data are needed as input for multizone air infiltration simulation codes, like the building site description, the air leakage network and the pressure coefficients. Other data are provided, such as air flow rates and differential pressures, which can be compared with the results of the codes.

The confidence interval of most of the measurements are also given in order to evaluate the result of this comparison, that is to decide if the fit is good or bad.

A part of this set was used once before its publication in a validation exercise, and has proved to be useable. This does not mean however that it can be used for any code in any case. Therefore, the following important points are remembered here:

- 1) The potential user should take liaison with the authors, first to obtain the data set on a magnetic tape or disc and secondly to get the data which are unintentionally forgotten in this paper.
- 2) The users are kindly requested to send their comments to the authors, in order to enhance the quality and the usability of this set

As the aim of this workshop is to finalize the structure of the Centre's database and explain data sources and needs, we give here some personal comments.

Infiltration codes steatily evoluate, taking into account more phenomenon as moisture and temperature gradients, air compressibility and turbulence effects. Nevertheless we would like to be simultaneously able to validate new codes with a data set. It is surely not an easy position; but before analysing some of its consequences we want to justify it.

The rapid evolution of the simulation codes is now mainly driven by the possibilities of the computers. Since there is very small experimental feedback, any new computer system allows to add new features to the codes without any information on either the necessity nor the accuracy of such new features. Moreover, it is not possible that way to ensure a good homogeneity in the accuracy of the various results of a given code. That code may have performant and accurate subroutines for some phenomena but be completely wrong for others.

स्यामा जाता.

We propose that the confrontation with measurements shall indicate the main directions to improve the codes. The measurements are certainly not perfect; they are contaminated with errors, as shown in reference [7], but measurements are the link with the reality and show the technical limits. Therefore, it does not appear necessary to calculate influences which cannot be measured.

Let us come back to the consequences of such a position. There is a need for an improvable data base. How to provide it?

On one hand it is not possible to add a later measurement in a time dependant data set. On another hand, experiences have shown that it is unrealistic to measure every possible physical quantity without knowing how these measurements will be used. It is well known that such type of data usually ends in the rubbish bin.

Our proposal is to keep some instrumented buildings ready for measurement, improving that way steadily the quality of the measurements.

So the data base could evaluate together with the codes, being an element of constant dialogue and not, as today a difficult examination whose result is seldom clear.

That proposal looks expensive but may not really be as expensive as the use of not completely validated codes. Nevertheless, it is surely less expensive that new comprehensive measurements and a new data base for each code.

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