42768

RESIDENTIAL COMBUSTION SPILLAGE MONITORING

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ABSTRACT

Sixteen homes were continuously monitored to determine the frequency and duration of combustion product spillage from the furnaces and DHW systems. In the houses which did show spillage activity, event-controlled sampling was used to determine levels of air contaminants attributable to the spillage.

Additional testing of the sample houses included: air tightness testing, air change rate testing and "forced spillage" contaminant testing.

DISCLAIMER

This project was funded by the Canada Mortgage and Housing Corporation and the Panel for Energy Research and Development (PERD), but the views expressed are the personal views of the authors, and neither the Corporation nor PERD accepts responsibility for them.

EXECUTIVE SUMMARY

In a previous research contract, Canada Martgage and Housing Corporation (CMHC) had simple monitors installed in approximately 900 houses to detect spillage of combustion products from fuel-fired furnaces and hot water heaters. In this study, CMHC found that a significant percentage of hauses did have occurrences of combustion product spillage from these appliances.

Buchan, Lawton, Parent Ltd. was contracted by CMHC to carry out a more detailed monitoring programme on sample houses which had experienced incidents of combustion spillage.

The methodology incorporated two basic elements. The first, carried out on all sixteen houses covered under the test pragramme, was to monitor the mechanical systems and door and window operation of the houses to determine the frequency and duration of spillage incidents, and the status of exhausting equipment and envelope openings during these incidents. Testing and recording of house details, such as envelope air leakage and occupancy characteristics, were also done.

The second element was air sampling to determine contaminant levels attributable to combustion product spillage from the appliances. Two sampling technologies were employed. Tube sampling methods were used for NO, NO2, and (in oil-heated houses and a limited number of gas-heated houses) SO2. As well, bag samples were collected for later analysis by gas chromatography for CO, CO2, methane and non-methane hydrocarbons. Three samples also underwent further analysis by mass spectrophotometry for a more complete analysis of organic compounds.

Air sampling was carried out in the houses as found, and during a period in which the combustion appliances were forced to spill by use of a high volume door fan. On those houses where significant 'naturally occurring' spillage events were recorded, a pump sampling package was installed, controlled by the monitoring system, which collected bag samples and, in a limited number of cases, NO₂ sorbant tube samples through two sampling trains. One sampling train collected only on spillage events and the other was activated on a time controlled basis, thus collecting an 'average' sample.

Monitoring activities were carried out in a total of sixteen houses, nine in Ottawa and seven in Winnipeg. Three of the Ottawa houses were oil-heated, the rest were heated by natural gas. Monitoring was done over a period of fourteen to thirty-five days on individual houses and a total of 322 days of usable monitoring data was gathered.

Of the sample sixteen houses, nine showed no spillage activity during the period they were monitored. Five gas-heated houses had significant spillage incidences and the remaining two houses, which were oil-heated, had brief, infrequent periods where spillage was detected.

In two of the houses which showed significant spillage occurrence, spillage was found to correlate with the operation of other exhausting appliances, a fireplace in one case and exhaust fans in the other. The three other spilled even without those aggrevating factors.

While some attempt has been made to correlate spillage data with atmospheric weather conditions (from Atmospheric Environment Service Weather Data), no direct correlation can be seen. This is not to say that there is no correlation, but rather, other factors such as exhaust appliance operation or poor chimney action overwhelmed weather effects.

Air quality sampling results indicate that there is some increase in contamination levels attributable to combustion spillage from the appliances, but that the increase was not dramatic.

It was found that during the forced spillage testing in some houses, contaminant levels, particularily carbon dioxide, did increase well above ambient levels (CO₂ concentrations up to 6636 ppm). In normal operation, even in those houses which spilled consistantly, the contaminant levels were below levels specified in existing standards and Health and Welfares proposed guidelines levels.

The study concludes that considering that the sample selection was limited to houses previously determined to have spillage occurrences, remarkably few had significant spillage incidents. Furthermore, while contaminant levels attributed to combustion product spillage were higher than ambient or average levels and in 'forced spillage' tests reached unacceptable levels, the contaminant levels from 'naturally occurring' spillage incidents were below Health and Welfare proposed guidelines.

It was noted, however, that the frequency and duration of combustion spillage and the levels of contaminants attributable to both 'forced' and 'naturally' occurring spillage were very house-specific. While hazardous levels of contaminants were not recorded from 'naturally' occurring spillage in the relatively few houses in which spillage was monitored, there is reason to suspect that in a limited number of cases, contamination levels could be a problem. The results would, however, indicate that this should be rare.

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I.O INTRODUCTION AND BACKGROUND

During the course of a number of previous projects, Canada Mortgage and Housing Corporation (CMHC) has been attempting to define the prevalence and impact of combustion product spillage in Canadian Houses. The most significant project was one which surveyed approximately 900 houses across Canada (Reference I). A simple temperature sensor was used to determine that combustion product spillage from furnace and hot water heaters had occurred in a significant percentage of the houses tested.

The technology used in the broad survey was limited in that it did not define the actual duration and number of occurrences of spillage, nor did it attempt to determine the effect of spillage on the indoor environment. These issues were addressed in the present project.

Buchan, Lawton, Parent Ltd.'s response to a CMHC request for proposals offered to carry out monitoring of a significant number of houses to determine the number and duration of spillage incidents, what household operation characteristics influenced spillage and the effect on the indoor environment. To meet objectives within CMHC's stated budget constraints required some innovation and planning, especially considering contract and heating season restraints limited all preliminary work and field monitoring to a period from contract award on January 16th 1987 until the end of the heating season which was deemed to be the end of March 1987.

This report is broken down into several sections. In section two one can find sub-sections discussing the selection of the case study houses, descriptions of the monitoring systems and methodology employed and a description of the air sampling methods used. Section three summarizes the field experience and the results of the program. Section four provides comments and conclusions.

Appendix A provides the data for each house on an individual basis.

2.0 PROCEDURES

The approach employed was to use "IBM PC clone" computer systems as an eight channel status data acquisition system by the use of a standard games controller card. Four of these channels were used to determine whether the combustion appliances were on or off and whether spillage was occurring. The other four determined house activity status, including whether or not windows and doors were open (on two sides split by orientation), whether exhaust fans were operating and whether the fireplace was in use.

This monitoring activity was carried out on nine houses in Ottawa and seven in Winnipeg. On those houses which showed significant spillage occurring, further work was undertaken to determine the effects of spillage on indoor air quality. This was done by using air sampling packages containing conventional aquarium pumps to draw air samples into mylar sample bags. The pumps were controlled by two output channels from the microcomputer. One pump was activated when a significant spillage event occurred and the other was on a regular time cycle so that "average" indoor contaminant levels could be determined.

Because of time and budget restraints, the project was limited to looking at "worst case" issues. The sample location was in an area near the furnace and near the ceiling (it was assumed that hot exhaust gases would tend to rise).

2.1 Unit Selection

The prime source of information on houses which had indications of spillage occurring was the data base built up by CMHC from previous projects. Initially, strong efforts were made to locate other spillage houses in the Ottawa area, as keeping the study within the Ottawa region would have a major impact on cost and flexibility.

CMHC supplied the names of nine houses that were "three dot failures" from their previous work (Reference I). Of these, five agreed to the detailed monitoring program described in this report. Four other houses, with spillage frequencies, were found through contacts with the contractors who had carried out the previous study and through heating service firms. It soon became quite evident that finding additional houses was going to be a problem under the very tight time constraints of the contract, especially since these houses had to be found at the time of year when spillage was assumed less likely to occur (cold weather with frequent winds). Buchan,

Lawton, Parent Ltd. was forced to look farther afield and made arrangements with G.K. Yuill and Associates in Winnipeg to contact some of the failure houses which had been located in Winnipeg during CMHC's previous work. Seven houses were found for the project in Winnipeg. BLP personnel went to Winnipeg to install the monitoring systems. On-site sampling and data gathering was carried out by personnel at G.K. Yuill and Associates.

House descriptions and data for each house covered in the program are included in Appendix A. Thirteen houses were gas heated and three were oil heated. Air quality monitoring was carried out in two of the oil heated houses and seven of the gas heated houses.

2.2 Monitoring Equipment

The key to providing the level of information required in this project at an acceptable cost was the use of standard microcomputers, specifically IBM PC clones, as the monitoring system. These were selected because they were readily available and inexpensive to rent. When equipped with dual floppy disk drives and a "multi-function card" (as they are normally available from suppliers), they have adequate storage capacity, the availability of a limited number of input channels (through the joystick controller portion of multi-function card), a real time clock (again on the multi-function card), and the ability to provide output signals (using the speaker connection and the "request to send" pin on the serial interface).

The monitoring systems and methods were designed around the capabilities and limitations of this building block. The games controller cards could provide four analog channels and four on-off status channels for data input. Because of some doubt about stability of the analog input, analog data recording was not attempted. On those sensors which provided analog signals, output was converted in software to status format based on field-settable threshold values. For example, when the measured resistance of a thermister fell below the set threshold, status was changed from off to on (cold to hot).

A description of the parameters measured and the type of sensors used are included in Table 2.1. It should be noted that some of the sensor selections were based on their availability within the time constraints, rather than selection of the best possible sensor for the application. If the equivalent system were to be used again, we would suggest some experimentation to see if thermistors could survive the undiluted flue

TABLE 2.1 MONITORING CHANNELS AND SENSORS

Channel	Channel Description
I, 2	Door and Window Status: These are monitored on two channels (north/west and south/east side of the house) by non-contact magnetic switches with external wiring. All sensors are ganged so that the information recorded is limited to whether or not any one window or door is open on either of the two sides of the building.
3	Fireplace Status: Measured with a thermostatic switch placed in the chimney, approximately 1.2 metres from the top, on a length of pyrotenax cable. The wiring is again external.
4	Fan Status: Monitored with FM intercom transmitters wired in parallel to the fan. When the fan is turned on, a signal is sent from the intercom transmitter to the receiving unit housed in the data acquisition package. This approach eliminated the need for internal wiring.
5	Furnace Status: For liability reasons, a decision was made to keep our installation non-intrusive to the furnace systems themselves. Furnace status was being measured by a temperature sensor just upstream of the dilution air inlet. For simplicity and availability, a simple 100k resistor was chosen as the sensor. This provided adequate signal differential and response time although its absolute accuracy was obviously not the same as a more conventional temperature sensor. However, the repeatability was acceptable, so all this required was an on-site software calibration.
6	Furnace Spillage: For gas units, the spillage condition was detected by a thermister at the dilution air inlet. On all oil-fired units, a smoke detector unit was used.
7	Domestic Hot Water Status: Operation was done in the same manner as furnace operation.
8	Domestic Hot Water Spillage: Spillage was sensed in the same manner as furnace spillage.

temperatures used to determine combustion appliance status. The simple and readily available sensors used (standard 100k resistors) worked adequately, but were the most unreliable component in the system.

One novel technique used during this study proved successful beyond our wildest expectations. This was the use of the FM intercoms to monitor exhaust fan status. There was only one house out of the sixteen in which this approach was not possible. The use of the intercoms eliminated the need for any internal wiring in the house. Costs associated with using the intercom were probably equal to the cost of wiring but the benefits in terms of home owner co-operation and convenience were tremendous.

It should be noted that using the standard games controller to accept card inputs from sensors was not entirely straight forward, requiring software elements such as software filtering and minimum trapping to obtain adequate signal reliability and response times.

There was some concern about the risk of leaving an open, unattended computer system in the monitored houses. Consequently, painted plywood boxes were fabricated to house the microcomputer and keyboard. The monitor was left exposed on top of the box because it provided output information which the homeowner was requested to relay to us during phone calls. The box also housed a connection board which contained terminals for all connections, the intercom receiver and the electronic circuitry required for signal conditioning of the other sensors.

2.3 Monitoring Software

The monitoring software used was a relatively simple program. It was developed by D. Marshall at SRO for this project, and written in BASIC, the program scanned all eight input panels and the clock on a continuous basis. On the analog channels, the signal was compared against thresholds for conversion to status output. Data was only written to disk when a change in status was noted and at this time the status of all eight channels was written to disk in one line.

The program also controlled two output signals (the speaker and "Request to Send" channel of the serial interface), which we used to control the air sampling pump package described in Section 2.4. The control software had user-definable settings for on-delays, off-delays and sampling pump run times.

The threshold values used to convert analog signals to status were also user-settable.

The program was self-booting so that if there was a power failure or any other interruption, the system would self-boot, losing a minimum of data. Interruptions were recorded on a separate data file.

A sample of the data is shown as Figure 2.1. Each column represents one channel matching from left to right the channel definitions of Table 2.1.

Data analysis routines were developed to scan through this data at a rapid pace to find spillage incidents providing the edited data shown in Figure 2.2 and to produce the summary tables described in Section 3.2.1.

2.4 Air Sampling Equipment and Procedures

There were basically three types of air sampling carried out during the course of the project.

On all houses, usually during installation of the data acquisition system, Gastec absorption tubes were used to check for the presence of NO₂, NO_X and, in some cases, SO₂. This was done at two locations in the house, the basement near the furnace and in the living space, usually in the master bedroom. These samples were taken before and during a period of spillage forced by the use of a door fan or blocking of the flue. In cases where detectable quantities of any of these contaminants were found during the forced spillage tests, additional tube samples were carried out at the same locations a few minutes after the forced spillage was stopped. Samples of air were collected in mylar bags from near the furnace. These were shipped to Mann Testing Laboratories where gas chromatography analysis was used to determine concentrations of CO, CO₂, methane and non-methane hydrocarbons.

On houses which were showing spillage within the first two weeks of monitoring, an air sampling package was installed. In each package there were two aquarium-type diaphram pumps controlled by outputs from the data acquisition system via solid state relays. Air drawn by these two pumps was collected in ten litre, coated, mylar sample bags. One pump activated when the data acquisition system detected a spillage condition longer than a user settable time delay (usually set at 15 seconds). This pump ran for the duration of the spillage incident and over a settable "off" delay after

FIGURE 2.1 Raw Data

Time	Doors & Windows s/e	Doors & Windows n/w	Fireplace	Fans	Furnace Status	Furnace Spillage	DHW Status	DHW Spillage	Pump 1 (Spillage Furn)	fump 2 (ambient indoor)
14:37:56 14:37:56 14:37:56 14:43:58 14:43:58 14:44:01 14:47:20 14:47:20 14:47:20 15:16:28 15:24:10 15:24:10 15:24:11 15:48:31 15:48:37 15:51:37 15:51:37 15:51:37 15:51:37 15:51:37 15:51:37 15:51:37 15:51:37 15:51:37 15:51:37 15:51:37 15:51:37 15:51:37 15:51:37 15:51:37 15:51:37 15:51:37	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000			0 0 0 0 1 0 0 0 0 0 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
15:56:08	0	1	1	1	1	0	1	0	0	0

03-14-1987 NEW DAY START EVENT 14:43:58
14:43:58 0 0 1 0<
14:44:01 0<
START EVENT FURN! DHW!PUMP! 15:16:25 0 0 1 1 0 0 0 0 15:16:28 0 0 1 1 1 0 0 0 0 15:16:33 0 0 1 1 1 0 0 0 0
START EVENT FURN! DHW!PUMP! 15:16:25 0 0 1 1 0 0 0 0 15:16:28 0 0 1 1 1 0 0 0 0 15:16:33 0 0 1 1 1 0 0 0 0
15:16:25
15:16:28
15:16:33 0 0 1 1 1 0 0 0 0
PUMP 1:EVENT 0.0 TOTAL 0.0 PUMP 2:TOTAL 0.0
START EVENT FURN! DHW!PUMP!
15:48:14 0 0 1 1 1 1 0 0 0 0
15:48:31 0 0 1 1 1 0 0 0 0
PUMP 1:EVENT 0.0 TOTAL 0.0 PUMP 2:TOTAL 0.0
START EVENT FURN! DHW!PUMP!
15:48:34 0 0 1 1 1 1 0 0 0 0
15:48:37 0 0 1 1 1 1 0 0 1 0
15:50:14 0 0 1 1 1 1 0 1 1 0
15:50:16
15:51:19 0 0 1 1 1 0 1 0 1 0
15:51:19 0 0 1 1 1 0 1 0 1 0 15:51:27 0 0 1 1 1 1 0 1 0 15:51:34 0 0 1 1 1 0 1 0
15:51:39 0 0 1 1 1 0 1 0 1 0
15:51:47

the incident ceased. The second pump was activated on a timed cycle and operated for 30 seconds every half hour. This pump was equipped with a metering valve and flow meter so that the flow rate could be set. The unrestricted flow rate of the pumps used was about one litre per minute which was deemed adequate for the spillage-controlled sample. For the timed sample it was adjusted to reduce this flow to approximately one half litre per minute to allow a 24 hour sample in the sample bag.

The bag samples were sent for analysis of CO, CO₂ and organics at Mann's testing lab in Toronto. A selected number of samples also underwent mass spectrography for a more complete analysis of the volatile organics.

It was recognized from the onset of this project that certain contaminants, notably nitrogen dioxide, could not be reliably analysed in a bag sample. Initial intentions were to draw samples through Gastec absorption tubes from the bags on-site, but even this was recognized as being somewhat unreliable because a sample could have been in the bag for up to 24 hours. With highly reactive nitrogen dioxide, this would be an excessive delay. While analysis for total oxides of nitrogen with Gastec tubes was also done, it was felt that, in those houses where significant spillage was occurring, it would be worthwhile to add additional effort to the nitrogen dioxide sampling. Consequently arrangements were made with the Ontario Research Foundation for the supply and analysis of a nitrogen dioxide sampler based on absorption of triethanolamine (TEA). These samplers are made up of three parts: the first contains a TEA impregnated molecular sieve which traps NO2, the second is an oxidizer section which converts all NO to NO, and the last contains the impregnated mollecular sieve which traps the converted NO2. Laboratory analysis to determine NO and NO2 concentrations was done at ORF.

These tubes use a pump sampling approach and the procedure required modification of two sample packages by the addition of two pumps mounted parallel to the original two.

Flow rates were set using flow valves to approximately one half litre per minute. Pump sampling time was controlled by the same logic as the bag sampling trains.

The computer program automatically determined pump run time so that the required sample volume calculation could be readily made. There was some startup instability in the pump flow rates. The flow meters used for setting flow rates had a specified accuracy of $\pm 10\%$ so there is some sample

volume errors but we judge it to be well within +20% accuracy levels desired for this project.

2.5 Other Testing

Two other procedures were carried out to provide support data for the spillage monitoring and air quality monitoring activities.

Each house was subject to a fan depressurization test according to CGSB/CAN 149.10M86. In the Ottawa houses, this was done by Buchan, Lawton, Parent Ltd. technologists and in Winnipeg the work was sub-contracted to NRG Industries Ltd. Results of the testing were recorded on the house data sheets in Appendix A.

As support for the air quality data, it is desirable to know the actual air change rate of the buildings during the monitoring period, consequently, a time-averaged tracer gas testing procedure developed by Brookhaven National Labs was employed. In this procedure, two sources of a perfluorocarbon tracer gas were located in each of two zones of the building, in the basement and in the master bedroom. The sources used in the two zones emit, at a relatively constant rate, different tracer gases so that inter-zone mixing can also be determined. A sampler which absorbs the tracer gases was mounted in the same rooms as the sources and left in place for the entire period that air quality monitoring was taking place. These samplers are analysed by a thermal desorption/mass spectrographic process, from which one can calculate a time-averaged air change rate and inter-zone mixing.

Supply and analysis of the samplers was sub-contracted to the National Association of Home Builders' (NAHB) Research Center in Upper Marlboro, MD.

3.0 RESULTS

3.1 Field Experiences and Problems

As with any project of this magnitude, a number of problems had to be overcome during the course of the monitoring program. It is worth noting them in order to facilitate future use of equivalent techniques and as a reference to help in explaining any data irregularities. Problems that were encountered included:

3.1.1 Appliance Status Sensors

Appliance status was monitored by measuring the resistance of 100k resistors placed in the flue, upstream of the dilution air inlet. The signal varied enough over the temperature range of a flue that a discrete status symbol could be obtained.

While a more direct acting sensor such as the relay on the furnace would seem more appropriate, there were real concerns over liability issues. Any problems with the furnace systems whether or not they were directly caused by our actions could be blamed on the monitoring system. It was decided to use temperature as the status indicator.

The resistors were chosen after some experimentation because they were available in the very short time frames required, they could be measured with the games controller card and they could survive the undiluted flue temperatures.

With hindsight, we feel that the high temperature thermistors (600°C), could be a more appropriate sensor but the only supplier of these sensors had too few thermistors in stock for both the status and spillage indicators needed.

The resistor's reaction time was much slower than the tiny thermistors (which were virtually instantaneous) used for the spillage indicators, so there was some sensor delay (in general about 15 seconds on both the on and off cycle). This delay has to be taken into account in any data analysis.

The change in resistance with temperature was not great (about 10 percent) between exposure to ambient and flue temperatures. There was a certain amount of trial and error in finding the correct threshold settings to obtain a positive response to status change. Otherwise, in a plateau region the computer recorded an event every two or three seconds which rapidly filled up the disk with data. This problem was accented by the

fact that the resistance sensors did drift significantly with time so field checking and calibration was necessary during site visits.

3.1.2 Inconsistent Output Signals

In this program sixteen different computers from three different suppliers were used at various times. All were IBM-PC clones, but there were some differences in how they were set up internally, notably with the speaker channel which was used as an output channel for the program. In the initial group of computers, we found that the output signal was strong, stable and acceptable for driving the solid state relay which turned on the sampling pumps.

In one of the latter systems in Ottawa and all of the systems in Winnipeg, it was found that this was not true. This channel produced a inconsistent signal creating varying pump flow rate. For the bag sampling this was not much of a problem since the measurement of bag samples were done based on concentration, so the absolute volume of samples didn't matter. On those houses where NO₂ sampling with the sorbent tube was used, knowledge of the actual pumped volume was critical. Plans included sampling for NO₂ on both spillage-controlled and timer-controlled sample trains. The inconsistent flow on the output used for the timer-controlled sample train reduced the NO₂ sampling to only one channel on two Winnipeg houses.

3.1.3 Sample Sizes

With the spillage controlled sample one can expect a great variation in sample size. A balance had to be drawn between sample volume flow and storage capacity. Ten and fifteen litre mylar bags were use for storage even though only about one litre was required for analysis. While there was some capacity to adjust the sample time delays and to a lesser extent, the flow rates, the time constraints of the project allowed only limited refinement of these parameters on an individual house. Because of the variation in sampling time, in some cases, unusably small samples were collected and, in other cases, bags were filled relatively rapidly, perhaps over one or two major spillage occurrences.

3.1.4 Lost Data

There were periods where data was lost. This can be traced to two sources.

In some cases, due to the problem described in section 3.1.1, disks were filled up much more rapidly than expected, and there was some elapsed time between the filling of the disks and site visits to replace them.

The second problem was encountered with the Winnipeg systems. On at least three occasions, the data could not be read from the disks. We suspect that it was some software compatibility problems in the operating system between the DOS system used in Ottawa and Winnipeg. In these cases, it was found that data was resident on the disks and could be read in a "block by block" fashion, however, the blocks were not always in chronological order. Procedures were set up to process the data in order to determine what happened over a period but the actual time of events was difficult to determine.

3.2 Monitoring Results

The basic data obtained in this project can be broken down into three categories: house and occupant characteristics, spillage frequency and duration data, and air quality data.

A summary of all data on a case study basis is included, by house, in Appendix A. For each house one will find:

- a description of the house and occupant characteristics including the floor plan,
- a series of tables analysing the operation and spillage data, and
- air quality sampling results.

Three types of tables are included to summarize operation and spillage data.

The first table shows the frequency and duration of significant spillage events. A significant spillage event was defined as 10 seconds of spillage (as determined from the spillage sensor) for a gas heated house and 5 seconds for an oil heated house.

The second table shows the effect of aggrevating conditions during spillage. In this table, the number of events and total time is binned in combinations of the aggrevating appliance status. These were defined as operation of the fireplace or woodstove, operation of any exhaust fans and the operation of the other fuel-fired appliance (furnace or DHW tank). The percentage of time that the house operated in any of the eight bin conditions is also shown. This allows assessment of the significance of

the spillage data in relation to total time. The last column in this table shows the number of spillage occurrences recorded when any of the windows or doors were open. This information should be used very carefully since the normal operation of the house in the winter is, of course, with the windows closed.

Air quality data is presented in a single table for each house. On this chart, you will find the results of all contaminant sampling, including results of tube-type sampling, bag samples or the pumped sorbent tube sampling far NO₂.

3.2.1. Operation and Spillage Data

Table 3.1 summarizes the number of monitored days, the number of days of data available and the number of days that were analysed in the above described charts of frequency, duration and aggrevating factors. A total of 363 days of monitoring was done. Approximately eleven percent of the data was lost due to problems mentioned in Section 3.1. Analysis for duration and aggrevating conditions data was only done on those disks where some spillage was recorded. This accounted for 96 days of data.

Of the five houses with spillage, it was very obvious that one (location code 02) spillage was almost exclusively driven by the fireplace. In fact, since the flue for the fireplace and the gas appliances are side by side, the fireplace smoke would get drawn down the appliance stack and into the house through the dilution air inlet of the gas DHW system.

In one other location (WI), the spillage seemed driven by other exhausting appliances, notably exhaust fans.

In three houses 03, 06 and W4, spillage occurred regularly, even in the absence of aggrevating conditions.

In two of the oil heated houses (05, 07), only short spillage incidents were recorded. This is consistent with the "startup puffs" one would expect with a powered burner system. There was some statistical correlation with aggrevating factors on a percentage of time basis but this spillage still occurred when the aggrevating factors were not present.

Figures 3.1 and 3.2 show how spillage occurrences correlate with AES weather data. On these plots, daily maximum and minimum temperature and

TABLE 3.1 MONITORING HISTORY

OTTAWA

Location Code	Oil Heated Houses	Spillage occurrence (N/Y)	Total Days Monitored	Days Data Available	Days Data Analysed
OI		N	16	16	0
02		Υ	28	27	12
03		Y	19	12	12
04	0	N	14	14	0
05	0	Υ	29	19	10
06		Υ	35	30	19
07	0	Υ	27	21	17
08		Ν	16	16	0
09		Ν	16	16	0
	Ottawa Totals		200	171	70
WINNIPE	G				
WI		Υ	33	33	11
W2		Ν	29	29	0
W3		Ν	16	16	0
W4		Υ	25	19	15
W5		Ν	28	28	0
W6		Ν	19	15	0
W7		Ν	13	11	0
,	Winnipeg Total	s	163	151	26
1	Project Totals		363	322	96

FIGURE 3.1

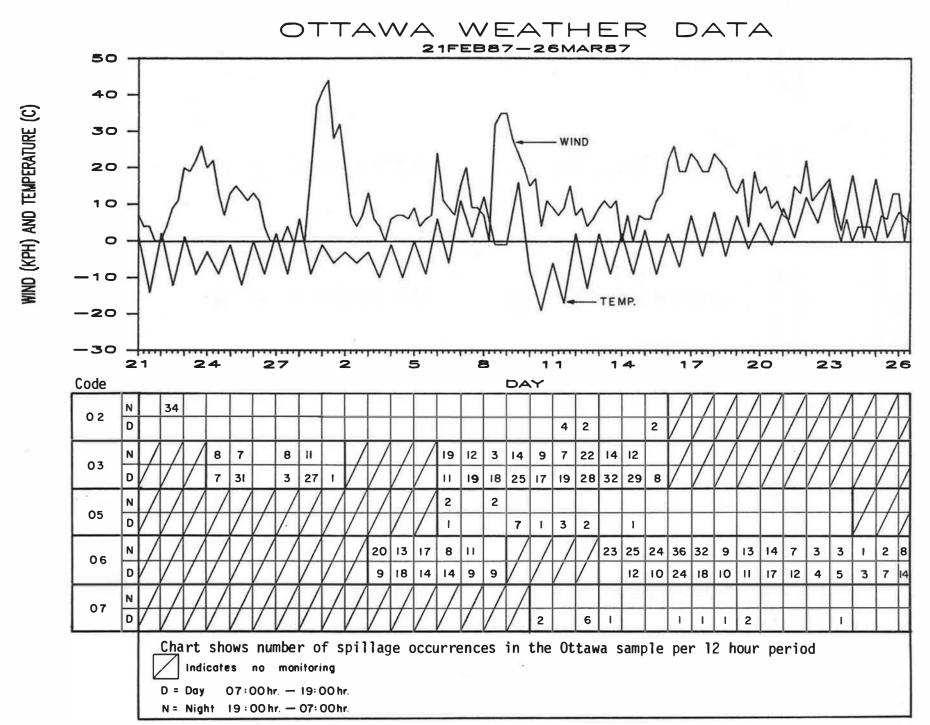
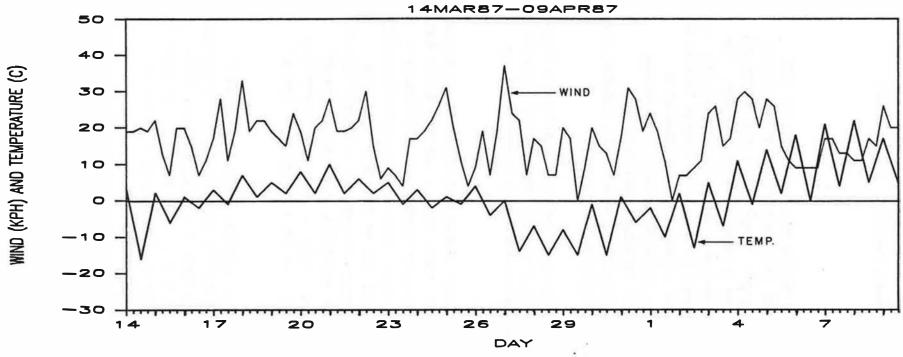
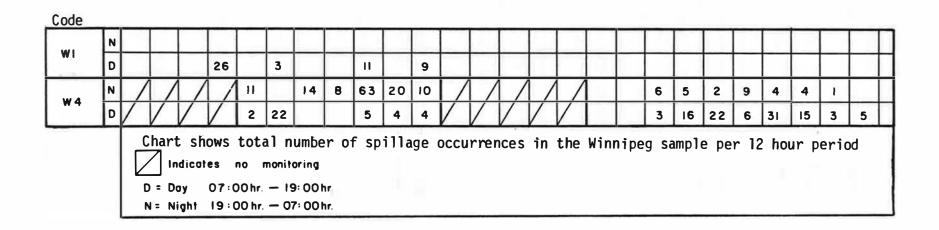


FIGURE 3.2

WINNIPEG WEATHER DATA





wind speed every six hours is plotted. Any direct correlation to wind and temperature is indiscernible with the data available. It is probably overwhelmed by other factors.

3.2.2 Air Quality Testing Results

Appendix A has a summary of quality testing results included for each house. The first three sections of this table show results of the Gastec tube-type sampling and gas chromotography sampling that was carried out before, during, and in some cases, after a period of forced spillage. The last two sections show results of the computer controlled sampling that was carried out in those houses which showed spillage. The samples labelled as "controlled" were drawn during spillage incidents and one labelled as "timed" was on a regular time cycling and could be considered average indoor levels. The computer controlled sampling consisted of gas chromotography analysis, in some cases NO/NO₂ sorbent tube sampling, and in three cases a more complete scan using mass spectography.

In a number of cases, it was impossible to do both a pre-spill and a forced spill bag sample because the long delivery time of bags from the supplier. In these cases only one sample was taken, the forced sample which was deemed more important.

Table 3.2 presents the maximum readings recorded on any of the 16 houses covered under the program. From this table, one can see that in the forced spillage tests, a fairly high reading of some contaminants, particularly CO_2 and SO_2 , were recorded but, in cases where naturally occurring spillage was monitored, contaminant levels would not be considered hazardous according to current standards and proposed Health and Welfare Guidelines. Interestingly, in many houses with the worst CO_2 levels during "forced" spillage did not spill during monitoring. Table 3.3 provides a comparison of "forced" and "natural" spillage results on those houses which did spill "naturally".

The results of the three samples which underwent mass spectographic analysis (Houses O2, O3, W4) are included in Appendix A with the relevant house. In general, levels of all VOC's were in the sub-parts per billion range, and no "concern" levels of any compound were found. The Mann Testing Laboratories' report is included as Appendix B. It should be noted, when viewing the sample results, that the SO₂ peak is the result of a system contaminant from the thermal desorption process and does not indicate the presence of this contaminant in the sample.

3.2.3 Air Change Testing Results

The NAHB-produced results of the long term tracer gas testing are included in Appendix C. The measured, overall air change for the tested houses were:

AC/h					
.263					
.239					
.010 *					
.688					
.449					
.329					
.378					
.229					

^{*} Impurities found in sample. Ignore result.

For detailed results, including inter-zone exchange rates, refer to Appendix C.

TABLE 3.2

MAXIMUM CONTAMINANT READINGS

		SORBEN	NT TUBE	SGA	BAG SAMPLES					
Spillage Type	Location	N0 ₂	N0	NO ₂	NO _X	SO ₂	CO	CO ₂	CH ₄	H.C*
		(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
Pre-spill	near furnace			0	0	0	1.9	1249	4	2.7
·	living space			0	0	0				
Forced	near furnace			0.6	7.5	0.2	5.3	6634	4.4	2.9
	living space			Trace	Trace	0.25				
Post Spill	near furnace			0	Trace	0.1				
·	living space			0	Trace	0.13				
Controlled	at furnace	0.76	0.366	-	-	-	3.7	1590	12.9	9.9
Timed	at furnace	0.58	0.079	-	-	-	2.7	983	7.7	5.1

^{*} H.C. - non methane hydrocarbons.

TABLE 3.3

COMPARISON OF 'FORCED' AND 'NATURAL'

SPILLAGE CONTAMINANT LEVELS

House Code	Forced/ Controlled	CO	CO ₂	CH ₄	H.C.
02	Forced Controlled	1.2 2.9-3.7	1826 697-1045	2.5 1.9-2.2	1.7 1.5 - 2.1
03	Forced	Bac	g Damaged in	Transit	
	Controlled	0.8-2.8	621-968	1.6-4.6	1.4-6.0
05	Forced	1.6	528	1.5	0.9
	Controlled	. 1.0	462	1.6	2.1
06	Forced	0.8	838	4.4	1.2
	Controlled	1.1-2.4	702-827	8.5-12.9	1.4-1.5
WI	Forced	0.1	503	2.8	2.9
	Controlled	0.8	646	2.5	2.7
W4	Forced	5.3	1 998	2.9	1.4
·	Controlled	0.5	570-1590	1.7-3.8	1.5-1.9

4.0 COMMENTS AND CONCLUSIONS

Although there were some problems expected during first time use of any field system, the low-cost, PC-based monitoring system used in the project worked remarkably well. We feel that this approach could be very useful for equivalent research projects, which require a limited amount of status-type data over a period in which capital and installation costs of a more complex data acquisition system are difficult to justify.

Considering that the houses monitored were pre-selected to be those in which spillage incidents were thought to have occurred, remarkably few actually had significant spillage events. While one could hypothesize that this was due to misleading data from the previous surveys, it is also likely that, for a large number of cases, the combination of environmental and house operation characteristics most condusive to the spillage are relatively rare, and that in the monitoring period, these conditions did not present themselves.

In examining the contributing factors to spillage problems, we are somewhat limited in our data. The possible correlation with temperature and wind effects is not immediately evident. The airtightness and air change testing data was collected to allow analysis of these effects. There has been no attempts at employing the results in correlations, as the effects of outside temperature and wind were marginal in the monitored houses. Applicance or venting system configuration and the effect of exhausting appliances are more strongly related to spillage incidents.

In two houses, spillage was directly related to the use of exhausting appliances. In three others, spillage commonly occurred even when exhausting appliances were off, suggesting that poor chimney action is the most important contributing factor.

In examining the effect of spillage on the indoor air quality, it is apparent, from the forced spillage testing that unacceptably high levels of some contaminants, particularily CO_2 and SO_2 , are possible when full spillage is occurring, as it was in our forced tests.

On the other hand, the observed effects of naturally occurring spillage were not dramatic. Results indicate a percentage rather than multiple increase in the levels of contaminants. None of the readings exceeded industrial standards or proposed Health and Welfare Guidelines for residential indoor air contaminant levels.

Therefore, while the forced testing would indicate that the potential for hazardous levels is possible, the monitoring results indicate that such hazardous levels should be rare.

REFERENCES

I. RESIDENTIAL COMBUSTION VENTING FAILURE - A SYSTEMS APPROACH Scanada Sheltair Consortium, for CMHC, 1987

APPENDIX A

House Data

LEGEND FOR AIR QUALITY

NO = Nitric Oxide

NO2 = Nitrogen Dioxide

NOx = other Oxides of Nitrogen

SO2 = Sulpher Dioxide CO = Carbon Monoxide CO2 = Carbon Dioxide

CH4 ≈ Methane

H.C.= Non Methane Hydrocarbons

02 = 0xygen

HOME PROFILE

- 1. HOUSE IDENTIFICATION: No. O-1
- 2. HOUSE DESCRIPTION:

Total Floor Area: 206 m², two storey, semi-detached

3. SPACE HEATING:

Fuel: natural gas Heat Distribution: forced air Location: open basement

4. DOMESTIC HOT WATER HEATING:

Fuel: natural gas
Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplace
Fuel: wood
Frequency of Use: once per winter month
Chimney Type: masonry

6. EXHAUST FANS FREQUENTLY USED:

clothes dryer bathroom central vacuum

7. DOORS/WINDOWS FREQUENTLY USED:

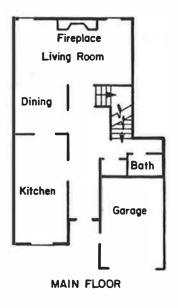
main entrance back door

8. FAN TEST CHARACTERISTICS:

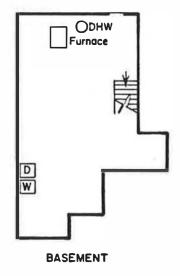
6.81 Air Changes per Hour (@ 50 Pa) 0.098 Equivalent Leakage Area (m²)

9. HOMEOWNER PROFILE:

Occupants 18 years and older: 4
Occupants under 18 years: 1
Number of occupants who smoke: 1









Air Analysis Results of Residential Combustion Spillage Monitoring

		Address: 0	1		С	ity: D	ttawa	F	uel Typ	e: G	as	
SPILLAGE Type	Date	Location	GAS NO2 (ppm)	STEC Tub NO× (ppm)	9es \$02 (ppm)	CO (ppm)	F CO2 (ppm)	Bag Samp CH4 (ppm)	les H.C (ppm)	02	Sorbent Tubes NO2 NO (ppm) (ppm)	Pump Time (sec.)
PRE SPILL	Feb II	At furnace Opp.end of bsmt	0	0 0								
FORCED	Feb 11	At furnace Opp.end of bsmt	0	0		1.1	750	4.4	0.9	21		
POST SPILL	Feb 11	At furnace Opp.end of bsmt.	0	0								

HOME PROFILE

- I. HOUSE IDENTIFICATION: No. 0-2
- 2. HOUSE DESCRIPTION:

Total Floor Area: 204 m², two storey, single detached

3. SPACE HEATING:

Fuel: natural gas
Heat Distribution: forced air
Location: open basement

4. DOMESTIC HOT WATER HEATING:

Fuel: natural gas Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplace
Fuel: wood
Frequency of Use: once per winter week
Chimney Type: masonry

6. EXHAUST FANS FREQUENTLY USED:

clothes dryer master bedroom bathroom upstairs bathroom

7. DOORS/WINDOWS FREQUENTLY USED:

main entrance side door kitchen windows

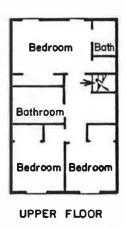
8. FAN TEST CHARACTERISTICS:

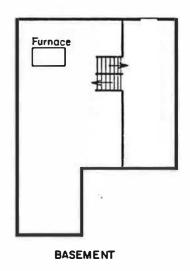
3.79 Air Changes per Hour (@ 50 Pa)0.070 Equivalent Leakage Area (m²)

9. HOMEOWNER PROFILE:

Occupants 18 years and older: 2
Occupants under 18 years: 0
Number of occupants who smoke: 1









Location Code:02 Start dote:10FEB87 End date:22FEB87 Total Number of Days Analyzed in these Tables: 4 Total Number of Days Monitored for this House:28

TABLE1: FREQUENCY AND DURATION OF SPILLAGE EVENTS

Spillage time Interval	Total Sp	illage	Events
(sec)	Furnace	DHM I	otal
10-29	0	21	21
30-120	0	. 9	9
>120	0	4	4
Total	0	34	34

TABLE 2:AGGRAVATING CONDITIONS DURING SPILLAGE EVENTS

List of Con			itions	% Time	Spilla	ae Events	Total	
Fi	replace	Fan	Other Devices	Condition True	Totals	Time(min)	Window Open Occurrences	
	OFF	OFF	OFF	87.724	0	0.00	0	
	OFF	NO	OFF	6.962	0	0.00	0	
	OFF	OFF	ON	0.746	0	0.00	0	
	OFF	ОN	ON	0.717	0	0.00	0	
	ON	OFF	OFF	3.737	31	34.25	1	
	DИ	מא	OFF	0.075	1	19.92	0	
	ON	OFF	ОN	0.037	1	0.18	0	
	DN	NO	ON	0.000	1	1.88	O	
				TOTAL	34	56		

note:column '% Time Condition True' has device status forced on if device is spilling

Location Code: O2 Start date:07hAP87 End date:15hAR87 Total Number of Days Analyzed in these Tables: 9 Total Number of Days Monitored for this House:28

TABLE1: FREQUENCY AND DURATION OF SPILLAGE EVENTS

Spillage time Total Spillage Events Interval

 (sec)	Furnace	DHW	Total	1	
 10-29	2		2	4	
30-120	0		0	0	
>120	2		2	4	
Iotal	4		4	8	

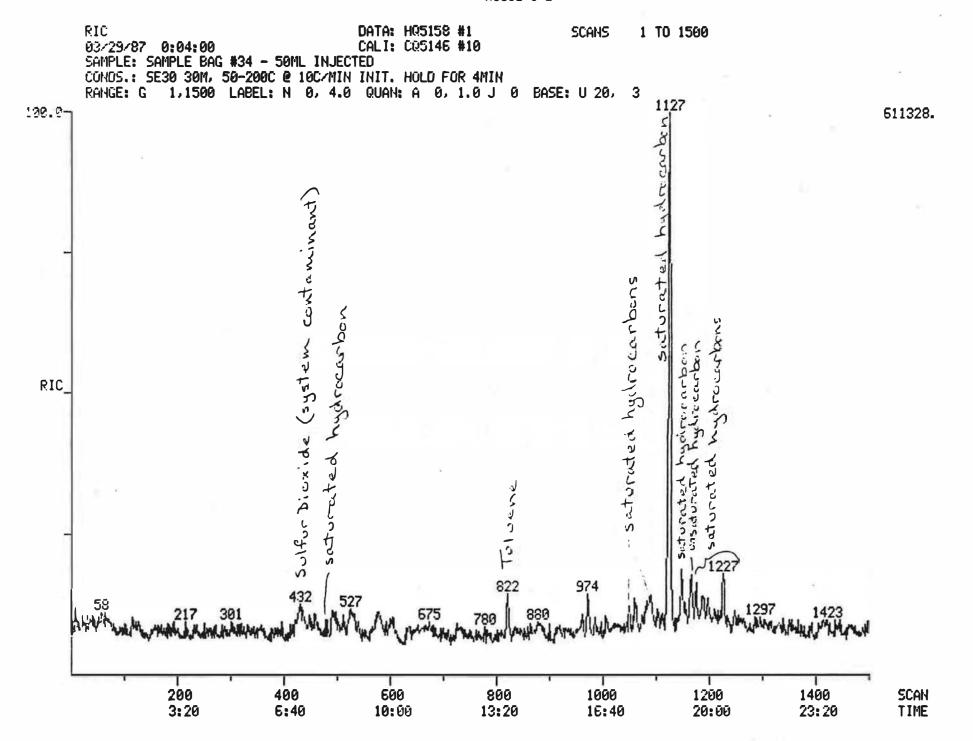
TABLE 2:AGGRAVATING CONDITIONS DURING SPILLAGE EVENTS

List of Condit Fireplace Fan		itions Other	% Time Condition	Spillad	e Events	Total Window Open	
		Devices	True	Totals	Time(min)	Occurrences	
OFF	OFF	OFF	80.388	1	0.25	0	
OFF	NO	OFF	4.401	0	0.00	0	
OFF	OFF	מס	0.222	0	0.00	- 0	
OFF	ОN	NO	0.481	0	0.00	0	
ОN	OFF	OFF	11.217	0	0.00	- 0	
ON	NO	OFF	3.034	4	22.50	2	
אם	OFF	ИО	0.000	0	0.00	0	
ON	NO	ON	0.257	3	41.37	2	
			TOTAL:	: 8	64		

note:column "% Time Condition True" has device status forced on if device is spilling

		Address: 0	12		C	ity: O	ttawa	F	uel Type	e: G	as		
SPILLAGE Type	Date _.	Location	GAS NO2 (ppm)	TEC Tub NOx (ppm)		CO	C02		ples H.C (ppm)	02	NO2	Tubes NO (ppm)	Pump Time (sec.
	R.1. 16												
PRE SPILL	Feb.16	beside furnace master bedroom	0	0	0								
FORCED	Feb.16	At furnace	0	0	0	1.2	1826	2.5	1.7	21			
		master bedroom	0	0									
POST SPILL	Feb.16	At furnace master bedroom	0	0									
CONTROLLED	Mar.12-14	At furnace				2.9	697	1.9	2.1	21			71
	Mar.14-16		M.S.X			3.7	1045	2.2	1.5	21			255
				A	/G.	3.3	871	2.05	1.8	21			
TIMED	Mar.12-14	At furnace				1.2	595	1.9	1.2	21			300
	Mar.14-16	•				1.3	600	1.9	1.7	21			180
				A	JG.	1.25	5 98	1.9	1.45	21			

NOTE : M.S. = MASS SPECTROMETER DONE.



- I. HOUSE IDENTIFICATION: No. 0-3
- 2. HOUSE DESCRIPTION:

Total Floor Area: 186 m², one storey, single detached

3. SPACE HEATING:

Fuel: natural gas

Heat Distribution: forced air

Location: enclosed furnace room

4. DOMESTIC HOT WATER HEATING:

Fuel: natural gas Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplace Type: woodstove Fuel: wood

Frequency of Use: once per year Frequency of use: daily

Chimney Type: masonry Chimney Type: insulated metal

6. EXHAUST FANS FREQUENTLY USED:

clothes dryer kitchen range

7. DOORS/WINDOWS FREQUENTLY USED:

main entrance kitchen door side door front bedroom

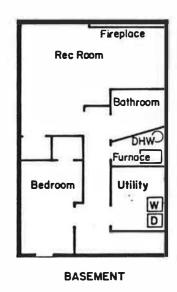
8. FAN TEST CHARACTERISTICS:

5.3 Air Changes per Hour (@ 50 Pa) 0.082 Equivalent Leakage Area (m²)

9. HOMEOWNER PROFILE:

Occupants 18 years and older: 4
Occupants under 18 years: 1
Number of occupants who smoke: 0







Location Code: 03 Start date:24FEB87 End date:26FFB87 Total Number of Days Analyzed in these Tables: 2 Total Number of Days Monitored for this House:19

TABLE1: FREQUENCY AND DURATION OF SPILLAGE EVENTS

Spillage time Interval	Total Sp	illage Ev	ents
(sec)	Furnace	IHW Tot	al
10-29 30-120 >120 Total	11 0 1 12	22 5 14 41	33 5 15 53

TABLE 2:AGGRAVATING CONDITIONS DURING SPILLAGE EVENTS

List of Fireplace		Other	% Time Condition	ำ		e Events	Total Window Open
		Devices	True	To	otals	Time(min)	Occurrences
OFF	ÜFF	OFF	14.650		3	0.73	0
OFF	หด	OFF	6.449		7	37.48	2
OFF	OFF	ОИ	0.855		1	0.17	1
OFF	140	ио	0.650		0	0.00	0
ИО	OFF	OFF	28.820		4	1.47	0
ОN	ИO	OFF	46.436		24	61.50	3
DИ	ÜFF	ON	1.887		9	15.27	3
ON	ON	אט	0.253		5	49.28	1
			TOT	AL:	53	166	

note:column "% Time Condition True" has device status forced on if device is spilling

Location Code:03

Start date:27FEB87 End date:O(MAR87 Total Number of Days Analyzed in these Tables: 2 Total Number of Davs Monitored for this House:19

TABLE1: FREQUENCY AND DURATION OF SPILLAGE EVENTS

Spillage time Total Spillage Events

(sec)	Furnace	DHW	Total
10-29	15	17	32
30-120	1	8	9
>120	0	9) 9
Total	16	34	50

TABLE 2:AGGRAVATING CONDITIONS DURING SPILLAGE EVENTS

List of Fireplace	_		% Time Condition True	•	ae Events Time(min)	Total Window Open Occurrences
OFF	ÜFF	OFF	 29.355	7	37.02	3
OFF	ÜN	OFF	28.465	7	2.22	1
				•		1
OFF	UFF	אם	0.235	5	2.82	0
OFF	אט	אט	0.131	2	20.43	0
DΝ	OFF	OFF	16.375	6	1.63	• 0
ОИ	ON	OFF	25.203	20	46.27	. 9
ИО	OFF	NO	0.028	0	0.00	0
ОИ	ИО	ON	0.208	3	3.28	0

TOTAL: 50 114

note:column "% Time Condition True" has device status forced on if device is spilling.

Location Code:03

Start date:06MAR87 End date:16MAR87

Total Number of Days Analyzed in these Tables: 9 Total Number of Days Monitored for this House:19

TABLE1: FREQUENCY AND DURATION OF SPILLAGE EVENTS

Spillage time Total Spillage Events Interval

7110C X 4 2 2			
(sec)	Furnace	DHW	Total
10-29	88	123	211
30-120	2	25	5 27
>120	0	80	80
Total	90	228	318

TABLE 2:AGGRAVATING CONDITIONS DURING SPILLAGE EVENTS

List of Con- Fireplace Fa			% Time Condition	Spilla	ge Events	Total Window Open		
		Devices	True	Totals	Time(min)	Occurrences		
OFF	OFF	OFF	70.229	182	490.02	42		
OFF	ИО	OFF	2.977	21	57.88	2		
OFF	ÜFF	אט	0.348	19	70.30	3		
OFF	ИÜ	אט	0.029	6	24.75	O		
ОИ	OFF	UFF	22.640	5 7	177.83	6		
ON	หย	OFF	3.602	21	61.00	1		
NO	OFF	ИО	0.144	12	28.65	5		
ON *	אַט	ио	0.031	0	0.00	0		

TOTAL: 318 910

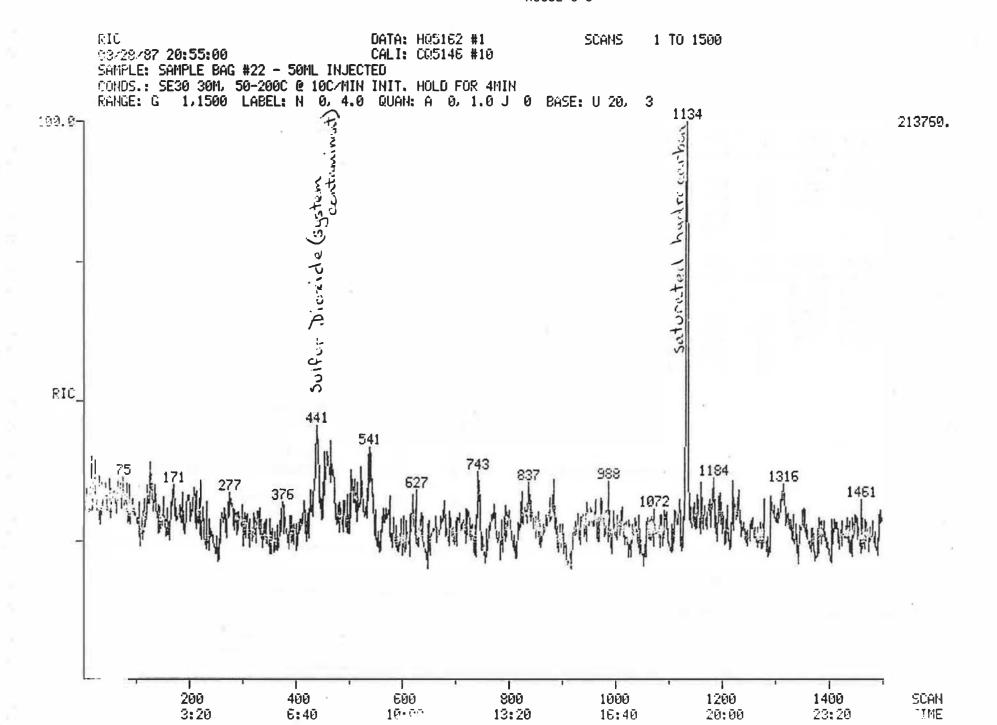
note:column '% Time Condition True' has device status forced on if device is spilling

Air Analysis Results of Residential Combustion Spillage Monitoring

		Address:	03		City: 0	ltawa	F	uel Tyo	e :	Gas		
SPILLAGE			GAS	TEC Tubes		1	Bag Samp	les		Sorbe	ent Tubes	Pump
TYPE	Date	Location	- NO2 (ppm)	NOx SO: (ppm) (ppm		CO2 (ppm)	CH4 (ppm)	H.C (ppm)	02 (%)	NO2 (ppm)	NO (ppm)	Time (sec.)
PRE SPILL	Feb.24	At furnace Living room	0	0 0	Trace	774	1.6	0.6	21			
FORCED	Feb.24	At furnace Living room	0.3	0	Sample b	oag dama	ged in	transit				
POST SPILL	Feb.21	At furnace Living room	0									
CONTROLLED	Mar.5-7 Mar.7-9	At furnace			2.8 1.8	937 968	4.3	6 5.1	21 21			3000 10420
	Mar.9-12		# M.S.#		0.8	621	1.6	1.8	21	N.D.	0.034	1254
	Mar.12-13	•	A 11151A		1.1	690	1.8	1.4	21		0.102	3483
	Mar.13-14	•								0.025	0.116	3724
	Mar.14-16	1								0.006	0.093	1244
				AVG.	1.625	804	3.1	3.6	21	0.011	0.086	
T IMED	Mar.5-7	At furnace			2.7	876	2.7	5.1	21			
111100	Mar.7-9	1			0.9	791	3	4.3	21			570
	Mar.9-12				0	534	3	1.5	21	N.D.	0.023	270
	Mar.12-13	• ==			1.1	687	2.4	1.5	21	0.007	0.058	660
	Mar.13-14									N.D.	0.079	600
				AVG.	1.2	722	2.85	3.1	21	0.007	0.053	

NOTE: N.D. = NONE DETECTED

M.S. = MASS SPECTROMETER DONE.



- I. HOUSE IDENTIFICATION: No. 0-4
- 2. HOUSE DESCRIPTION:

Total Floor Area: 250 m², one storey, single detached

3. SPACE HEATING:

Fuel: oil

Heat Distribution: forced air Location: open basement

4. DOMESTIC HOT WATER HEATING:

Fuel: electric

Location: basement

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplace

Fuel: wood

Frequency of Use: once per winter week

Chimney Type: masonry

6. EXHAUST FANS FREQUENTLY USED:

none

7. DOORS/WINDOWS FREQUENTLY USED:

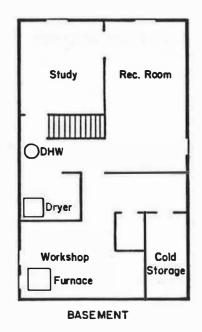
main entrance side door

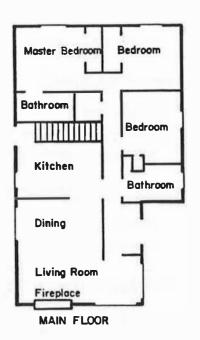
8. FAN TEST CHARACTERISTICS:

4.26 Air Changes per Hour (@ 50 Pa) 0.082 Equivalent Leakage Area (m²)

9. HOMEOWNER PROFILE:

Occupants 18 years and older: 3
Occupants under 18 years: 0
Number of occupants who smoke: 0





North ___

0 5m

	- 1	Address: 0	14	14.		C	ity: O	ttəwa	Fu	el Type	e: Oi	.1		
SPILLAGE			_	GAS	TEC Tul	es		F	ag Samp	les		Sorbent	Tubes	Pump
TYPE	Date ,	Location		ND2 ppm)	NOx (ppm)	SD2 (ppm)	(bbw)	CO2 (ppm)	CH4 (ppm)	H.C (ppm)	02 (%)		NO (ppm)	Time (sec.)
PRE SPILL	Feb.27	At furnace Living room		0	0 0	0					e 5			
FORCED	Feb.27	At furnace Living room		0	0	0.2 0.25	1.6	1904	1.1	0.9	21			
POST SPILL	Feb.27	At furnace Living room				0.1 0.13								

- I. HOUSE IDENTIFICATION: No. 0-5
- 2. HOUSE DESCRIPTION:

Total Floor Area: 180 m², suburban, two storey, semi-detached

3. SPACE HEATING:

Fuel: oil

Heat Distribution: forced air Location: enclosed basement

4. DOMESTIC HOT WATER HEATING:

Fuel: oil

Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplace

Fuel: wood

Frequency of Use: never Chimney Type: masonry

6. EXHAUST FANS FREQUENTLY USED:

main bathroom

range hood

basement bathroom

clothes dryer

7. DOORS/WINDOWS FREQUENTLY USED:

main entrance garage door

back bedroom window

8. FAN TEST CHARACTERISTICS:

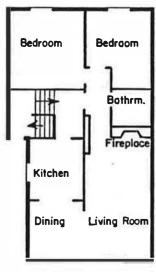
7.98 Air Changes per Hour (@ 50 Pa) 0.137 Equivalent Leakage Area (m²)

9. HOMEOWNER PROFILE:

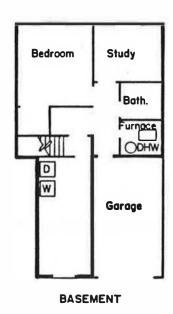
Occupants 18 years and older: 3

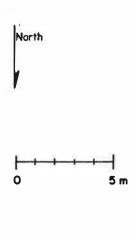
Occupants under 18 years: 0

Number of occupants who smoke: 1



MAIN FLOOR





HOUSE O-5

Location Code: OS Start date: OGMAR87 End date: O9MAR87 Total Number of Days Analyzed in these Tables: 3 Total Number of Days Monitored for this House: 29

TABLE1: FREQUENCY AND DURATION OF SPILLAGE EVENTS

Charles .

Spillage time Total Spillage Events Interval

				2.15
(sec)	Furnace	DHM	Tot	al
5-29	11		0	11
30-120	0		0	0
>120	0		0	0
Total	11		0	11

TABLE 2:AGGRAVATING CONDITIONS DURING SPILLAGE EVENTS

List of			% Time	Spillag	ge Events	Total
Fireplace	Fan	Other	Condition			Window Open
		Devices	True	Totals	Time(min)	Occurrences
OFF	ÜFF	OFF	94.005	7	0.90	1
			The state of the s			<u>.</u>
OFF	ИО	OFF	5.995	4	0.62	4
OFF	OFF	ИО	0.000	0	0.00	0
OFF	ИO	ON	0.000	0	0.00	0
ОИ	ÜFF	ÜFF	0.000	0	0.00	0
ON	ON	OFF	0.000	0	0.00	0
рM	OFF	ИО	0.000	0	0.00	0
ИО	ОИ	ЙN	0.000	0	0.00	0
			TOTAL:	11	2	

note:column '% Time Condition True' has device status forced on if device is spilling

Location Code:05 Start date:09MAR87 End date:15MAR87 Total Number of Days Analyzed in these Tables: 6 Total Number of Days Monitored for this House:29

TABLE1: FREQUENCY AND DURATION OF SPILLAGE EVENTS

4.

Spillage time	rorar 2b;	riigäe pae	PULS
Interval		*	
(sec)	Furnace	DHW Tota	1
5-29	5	3	8
30-120	0	0	0
>120	0	0	0
Total	5	3	8

TABLE 2:AGGRAVATING CONDITIONS DURING SPILLAGE EVENTS

List of Fireplace			% Time Condition	Spillad	e Events	Total Window Open
		Devices	True	Totals	Time(min)	Occurrences
OFF	OFF	OFF	97.893	1	0.10	0
OFF	ОN	OFF	1.950	0	0.00	0
OFF	OFF	ИО	0.156	6	0.55	0
OFF	ИО	ON	0.001	1	0.13	0
ИО	OFF	OFF	0.000	0	0.00	0
٥N	ÜN	OFF	0.000	0	0.00	0
ดพ	OFF	ИО	0.000	0	0.00	0
ON	ON	אס	0.000	0	0.00	0
			TOTAL	. 8	1	

note:column "% Time Condition True" has device status forced on if device is spilling

		Address:	05		C	ity: O	ttawa	F	uel Tyc	e: (Dil	
SPILLAGE TYPE Date	Location	GAS NO2 (ppm)	NO×	9es SO2 (ppm)	CO (ppm)	CO2 (ppm)	łag Samp CH4 (ppm)	H.C (ppm)	02	Sorbent Tubes NO2 NO (ppm) (ppm)	Pump Time (sec.	
PRE SPILL	Feb.25	At furnace Dining room	, 0 , 0	0 0	0	1.2	639	1.6	0.6	21		
FORCED	Feb.25	At furnace Dining room	0 0	0	0	1.6	528	1.5	0.9	21		
POST SPILL												
CONTROLLED	Mar.9-20	At furnace				1	462	1.6	2.1	21		70
TIMED	Mar.9-20	At furnace				1.9	513	1.7	3.6	21		120

- I. HOUSE IDENTIFICATION: No. 0-6
- 2. HOUSE DESCRIPTION:

Total Floor Area: 317 m², two storey, single detached

3. SPACE HEATING:

Fuel: natural gas

Heat Distribution: forced air Location: enclosed furnace room

4. DOMESTIC HOT WATER HEATING:

Fuel: natural gas

Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplace

Fuel: wood Fuel: wood

Frequency of Use: Frequency of use:

once per winter month three times per winter

Chimney Type: masonry Chimney Type: insulated metal

Type: wood stove

6. EXHAUST FANS FREQUENTLY USED:

main bathroom range hood

kitchen - Jenn Air clothes dryer

7. DOORS/WINDOWS FREQUENTLY USED:

main entrance back door

garage door five windows

8. FAN TEST CHARACTERISTICS:

7.01 Air Changes per Hour (@ 50 Pa)

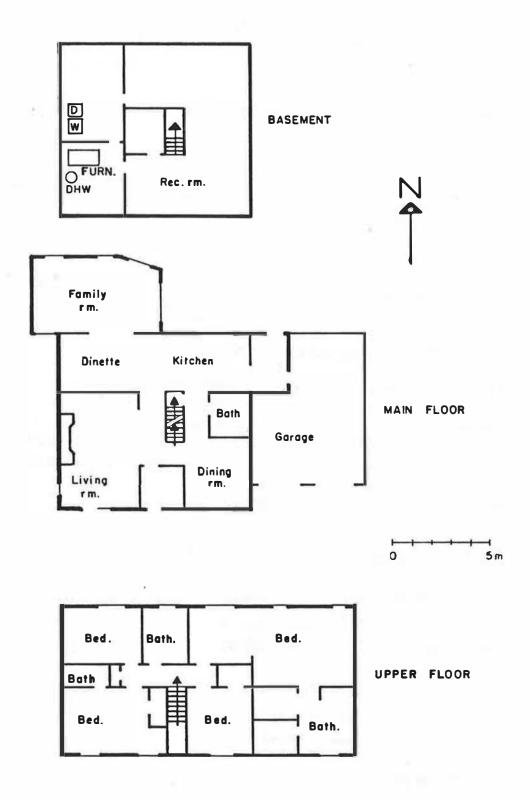
0.176 Equivalent Leakage Area (m²)

9. HOMEOWNER PROFILE:

Occupants 18 years and older: 2

Occupants under 18 years: 2

Number of occupants who smoke: 0



HOUSE O-6

Location Code:06 Start date:03MAR87 End date:08MAR87 Total Number of Days Analyzed in these Tables: 5 Total Number of Days Monitored for this House:35

TABLE1: FREQUENCY AND DURATION OF SPILLAGE EVENTS

Spillage time	Total	Spillage	Events
Interval			
(sec)	Furnac	e lihii	Total

(sec)	Eurnace	MHű	Tot	al
10.00	AE		^	
10-29	45 87	1	0	55 07
30-120 >120	87		0	87
Total	132	1	0	142

TABLE 2:AGGRAVATING CONDITIONS DURING SPILLAGE EVENTS

List of (Fireplace			% Time Condition	Spilla	ge Events	Total Window Open
		Devices	True	Totals	Time(min)	Occurrences
OFF	OFF	OFF	89.747	129	67.53	22
OFF	ИÜ	OF F	6.356	9	4.57	2
OFF	ÜFF	אס	2.455	1	0.23	0
OFF	ИÜ	אס	1.443	3	0.80	- 0
ON	ÜFF	OFF	0.000	0	0.00	0
ON	ИO	ÜFF	0.000	0	0.00	0
οN	OFF	ОN	0.000	0	0.00	0
NO	OM	אט	0.000	0	0.00	0
			ተበተለ፣	1 40	72	

TOTAL: 142 73

note:column "% Time Condition True" has device status forced on if device is spilling

Location Code:06

Start date:13MAR87 End date:27MAR87

Total Number of Days Analyzed in these Tables:14 Total Number of Days Monitored for this House:35

TABLE1: FREQUENCY AND DURATION OF SPILLAGE EVENTS

Spillage time Total Spillage Events
Interval

(sec)	Furnace	WНЩ	Total
10-29	121	20	141
30-120	204	4	208
>120	0	() 0
Total	325	24	349

TABLE 2:AGGRAVATING CONDITIONS DURING SPILLAGE EVENTS

List of			% Time	Spilla	ae Events	Total
Fireplace	Fan	Other Devices	Condition True	Totals	Time(min)	Window Open Occurrences
OFF	OFF	OFF	94.364	319	166.78	60
OFF	אס	OFF	4.250	11	4.50	7
OFF	ÜFF	אם	0.831	16	8.82	8
OFF	אט	אט	0.555	3	1.52	3
OΝ	OFF	OFF	0.000	0	0.00	0
NO	ОN	OFF	0.000	0	0.00	()
OΝ	ÜFF	אם	0.000	0	0.00	0
OM	ИО	ON	0.000	0	0.00	0

TOTAL: 349 182

note:column "% Time Condition True" has device status forced on if device is spilling

	200	Address:	06		C	ity: 0	ttawa	F	uel Typ	e:	Gas		
SPILLAGE Type	Date .	Location	NO2		S02	CO (ppm)	CO2 (ppm)	9ag Samp CH4 (ppm)		02	Sorbe NO2 (ppm)	nt Tubes NO (ppm)	Pump Time (sec.
PRE SPILL	Feb.21	At furnace Master bedroom	0 0	0 0		0.8	845	4	1.2	21			
FORCED	Feb.21	At furnace Master bedroom	0	0	0	0.8	838	4.4	1.2	21			
POST SPILL													
CONTROLLED	Mar.18-19 Mar.19-21 Mar.21-23	At furnace		4		1.6 2.4 1.1	762 827 702	12.9 7.3 8.5	1.5 1.4 1.4	21 21 21	0.019 0.006 0.025		957 3321 1242
od!				A	vg.	1.7	764	9.6	1.4	21	0.017	0.111	
T IMED	Mar.19-21	At furnace				1.1	578	7.7	1.7	21	0.0006	0 069	720 570

- I. HOUSE IDENTIFICATION: No. 0-7
- 2. HOUSE DESCRIPTION:

Total Floor Area: 288 m², duplex (upper floor, lower floor)

3. SPACE HEATING:

Fuel: oil
Heat Distribution: forced air
Location: enclosed furnace room

4. DOMESTIC HOT WATER HEATING:

Fuel: electric Location: in basement

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplaces (2)
Fuel: wood
Frequency of Use: twice per winter month
Chimney Type: masonry

6. EXHAUST FANS FREQUENTLY USED:

none

7. DOORS/WINDOWS FREQUENTLY USED:

main entrance door lower unit - side door

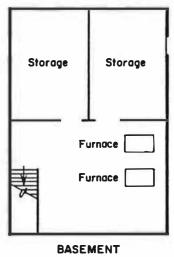
8. FAN TEST CHARACTERISTICS:

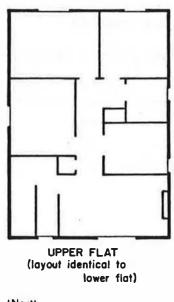
Access Refused For One Time Testing

9. HOMEOWNER PROFILE:

Occupants 18 years and older: 3
Occupants under 18 years: 0
Number of occupants who smoke: 2











Location Code:07 Start date:10MAR87 End date:27MAR87

13,500

Total Number of Days Analyzed in these Tables:17 Total Number of Days Monitored for this House:27

TABLE1: FREQUENCY AND DURATION OF SPILLAGE EVENTS

Spillage time Total Spillage Events Interval

THICETAGI			
(sec)	Furnl	Furn2 Tot	al
5-29	14	0	14
30-120	1	0	1
>120	0	0	0
Total	15	0	15

TABLE 2:AGGRAVATING CONDITIONS DURING SPILLAGE EVENTS

	ist of (replace			% Time Condition	Spilla	ae Events	Total Window Open
			Devices	True	Totals	Time(min)	Occurrences
17/10/10	OFF	ÜFF	OFF	99.591	13	1.77	0
	OFF	ИU	OFF	0.000	0	0.00	0
	OFF	OFF	ИО	0.409	2	0.22	0
	OFF.	ОИ	ÜN	0.000	0	0.00	0
	OΝ	ÜFF	ÜFF	0.000	0	0.00	0
	ОИ	ИО	OFF	0.000	0	0.00	0
	OΝ	OFF	ИО	0.000	0	0.00	0
	ON	OM	אט	0.000	0	0.00	O
				TOTAL	: 15	2	

note:column "% Time Condition True" has device status forced on if device is spilling

Air Analysis Results of Residential Combustion Spillage Monito	oring	Monitor	Spillage	bustion	1 (Residenti	of	Results	Analysis	Air
--	-------	---------	----------	---------	-----	-----------	----	---------	----------	-----

Address: 07 City: Ottawa Fuel Type: Oil

SPILLAGE ---GASTEC Tubes----Sorbent Tubes Pump TYPE ---Location---- NO2 NОх CO CO2 CH4 H.C NO2 Date S02 Time (ppm) (ppm) (ppm) (ppm) (ppm) (ppm) (%) (mqq) (mqq) (sec.)

PRE SPILL

FORCED

Access Refused For One Time Testing

POST SPILL

- I. HOUSE IDENTIFICATION: No. 0-8
- 2. HOUSE DESCRIPTION:

Total Floor Area: 278 m², one storey, single detached

3. SPACE HEATING:

Fuel: natural gas
Heat Distribution: forced air
Location: enclosed furnace room

4. DOMESTIC HOT WATER HEATING:

Fuel: natural gas Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplace Fuel: wood

Frequency of Use: never Chimney Type: masonry

6. EXHAUST FANS FREQUENTLY USED:

clothes dryer

7. DOORS/WINDOWS FREQUENTLY USED:

main entrance garage door

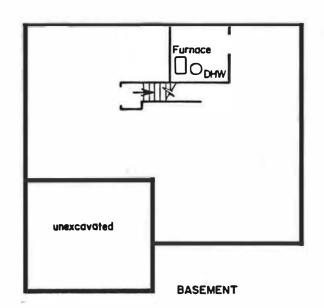
8. FAN TEST CHARACTERISTICS:

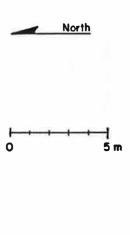
2.29 Air Changes per Hour (@ 50 Pa)0.056 Equivalent Leakage Area (m²)

9. HOMEOWNER PROFILE:

Occupants 18 years and older: 2
Occupants under 18 years: 0
Number of occupants who smoke: 0







HOUSE O-8

		Address:	08			City:	Ottawa		Fuel Ty	oe:	Gas	
SPILLAGE TYPE	Date .	Location	GASTE - NO2 (ppm)	NOx	5 502 (ppm)	CO	Baq CO2 (ppm)	Sampl CH4 (ppm)	Ps H.C (ppm)	02 (%)	Sorbent Tubes NO2 NO (ppm) (ppm)	Pump Time (sec.)
PRE SPILL	Mar.4	At furnace Living room	0 0	0 0		trace	696	2.6	1.2	21		
FORCED	Mar.4	At furnace Living room	0.1 0	4 0		NU	>6634.	1.4	1.2	21		
POST SPILL	Mar.4	At furnace By HRV vent	0 0 t	0 race								

ND = None Detected

- I. HOUSE IDENTIFICATION: No. 0-9
- 2. HOUSE DESCRIPTION:

Total Floor Area: 132 m², two storey, single detached

3. SPACE HEATING:

Fuel: natural gas

Heat Distribution: forced air Location: enclosed furnace room

4. DOMESTIC HOT WATER HEATING:

Fuel: natural gas

Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplace

Fuel: wood

Frequency of Use: twice per winter week

Chimney Type: insulated metal

6. EXHAUST FANS FREQUENTLY USED:

clothes dryer

main bathroom

upstairs bathroom

range hood

7. DOORS/WINDOWS FREQUENTLY USED:

main entrance

rear door

kitchen window

two bedroom windows

8. FAN TEST CHARACTERISTICS:

3.97 Air Changes per Hour (@ 50 Pa) 0.067 Equivalent Leakage Area (m²)

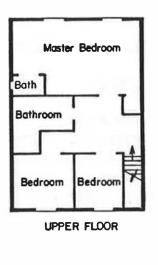
9. HOMEOWNER PROFILE:

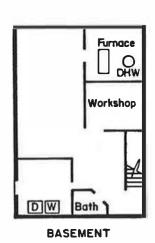
Occupants 18 years and older: 2

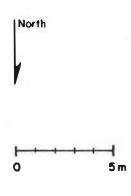
Occupants under 18 years: 0

Number of occupants who smoke: 0









PRE SPILL Mar.2 At furnace 0 0 trace 593 2.2 1.7 21 FORCED Mar.2 At furnace 0 0 trace >2594 2.2 1.7 21			Address:	09		City:	Ottawa	1	Fuel Ty	pe:	Gas	
(ppm) (ppm) (ppm) (ppm) (ppm) (ppm) (ppm) (ppm) (ppm) (sec. PRE SPILL Mar.2 At furnace 0 0 trace 593 2.2 1.7 21 Main floor hall 0 0 FORCED Mar.2 At furnace 0 0 trace >2594 2.2 1.7 21		Date	1003ti00									•
Main floor hall 0 0 FORCED Mar.2 At furnace 0 0 trace >2594 2.2 1.7 21	1112	pace .	Location									 (sec.)
Main floor hall 0 0 FORCED Mar.2 At furnace 0 0 trace >2594 2.2 1.7 21	PPE SPILL	Mar 2	At furnace	0	0	 trace	592	2.2	1 7	21		 ,
	11.0 31 200	113.12		*		01322	070	3.2	11,	21		
Main Flags ball () ()	FORCED	Mar.2	At furnace Main floor hall	0	0	trace	>2594	2.2	1.7	21		

PROFILE PAGE

- I. HOUSE IDENTIFICATION: No. W-1
- 2. HOUSE DESCRIPTION:

Total Floor Area: 150 m², two storey, semi-detached

3. SPACE HEATING:

Fuel: natural gas Heat Distribution: forced air Location: open basement

4. DOMESTIC HOT WATER HEATING:

Fuel: natural gas

Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplace Fuel: wood

Frequency of Use: once per winter month

Chimney Type: masonry

6. EXHAUST FANS FREQUENTLY USED:

first floor bathroom second floor bathroom clothes dryer

7. DOORS/WINDOWS FREQUENTLY USED:

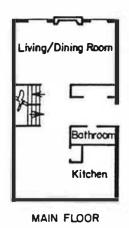
main entrance kitchen window

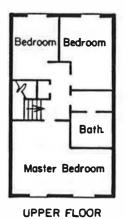
8. FAN TEST CHARACTERISTICS:

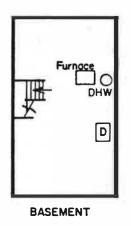
4.51 Air Changes per Hour (@ 50 Pa)
0.046 Equivalent Leakage Area (m²)

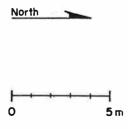
9. HOMEOWNER PROFILE:

Occupants 18 years and older: 2
Occupants under 18 years: 3
Number of occupants who smoke: 2









Location Code: W/

Start date:14mar87 End date:25mar87

Total Number of Days Analyzed in these Tables:11

Total Number of Days Monitored for this House:33

TABLE1: FREQUENCY AND DURATION OF SPILLAGE EVENTS

Spillage time Interval	Total Sp	illage Ev	ents
(sec)	Furnace	DHW Tot	al
10-29	0	33	33
30-120	O	10	10
>120	O	6	6
Total	Ō	49	49

TABLE 2: AGGRAVATING CONDITIONS DURING SPILLAGE EVENTS

List of Fireplace			% Time Condition True		e Events Time(min)	Total Window Open Occurrences
OFF	OFF	OFF	89.998	0	0.00	0
OFF	MO	OFF	8.183	26	14.82	0
OFF	OFF	ON	1.195	4	2.45	0
OFF	ON	OM	0.623	19	34.57	1
ONI	OFF	OFF	0.000	0	0.00	Q
DN	ОИ	OFF	0.000	0	0.00	0
ON	OFF	ON	0.002	0	0.00	Ō
ON	ОN	ØИ	0.000	0	0.00	. 0
			TOTAL:	4.5	52	

note:column "% Time Condition True" has device status forced on if device is spilling

Air Analysis Results of Residential Combustion Spillage Monitoring

		Address: W	1		Ci	ty: Wi	nnipea	Ein	el Type	: Gas			
SPILLAGE TYPE	Date .	Location	ND2			CO	C02	CH4	1es H.C (ppm)	02	NO2	NO	Pump Time (sec.)
PRE SPILL	Mar.14	At furnace In living room	0	0		0.5	744	1.9	1.5	21			
FORCED	Mar.14	At furnace In living room	. 0 0	0		0.1	563	2.8	2.9	21			
POST SPILL	Mar.14	At furnace In living room	0 0	0 0									
CONTROLLED	Mar.31 - ADr.2 Apr.2-16	At furnace				0.8	646	2.5	2.7 AV	0.	.032 0 .038 0 		225 1398
TIMED	Mar.31 - Apr.2	At furnace				1.4	593	2.6	2.5	21			120

HOME PROFILE

- I. HOUSE IDENTIFICATION: No. W-2
- 2. HOUSE DESCRIPTION:

Total Floor Area: 170 m², one storey, single

3. SPACE HEATING:

Fuel: natural gas
Heat Distribution: forced air
Location: open basement

4. DOMESTIC HOT WATER HEATING:

Fuel: natural gas
Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: none
Fuel: n/a
Frequency of Use: n/a
Chimney Type: n/a

6. EXHAUST FANS FREQUENTLY USED:

bathroom central vacuum clothes dryer

7. DOORS/WINDOWS FREQUENTLY USED:

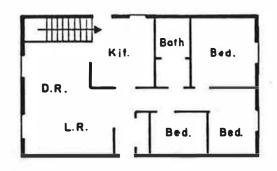
main entrance kitchen entrance

8. FAN TEST CHARACTERISTICS:

2.07 Air Changes per Hour (@ 50 Pa) 0.034 Equivalent Leakage Area (m²)

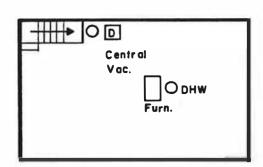
9. HOMEOWNER PROFILE:

Occupants 18 years and older: 2
Occupants under 18 years: 2
Number of occupants who smoke: 0



GROUND FLOOR





BASEMENT



Air Analysis Results of Residential Combustion Spillage Monitoring

			12		C	ity: W	INNIPEG	Fu	sel Type	e: Ga	95		
SPILLAGE		5.87	GAS	TEC Tut	es			ag Samp	les		Sorbent	Tubes	Pump
TYPE	Date	Location	NO2 (mgg)	NOx (ppm)	\$02 (ppm)	CO (pom)	CO2 (ppm)	CH4 (ppm)	H.C (ppm)	(%)	NO2 (ppm)	NO (ppm)	Time (sec.)
DDE CDIII	M 16					Λ.	1076						
PRE SPILL	Mar _, 16	near furnace living room	0	0		0.5	1076	1.7	1.2	21			
FORCED	Mar 16	near furnace	0.6	0		0.5	963	1.8	1.5	21			
		living room	0	0									
POST SPILL	Mar 16	near furnace	0	0									
		living room	0	0									

HOME PROFILE

- I. HOUSE IDENTIFICATION: No. W-3
- 2. HOUSE DESCRIPTION:

Total Floor Area: 321 m², one storey, single detached

3. SPACE HEATING:

Fuel: natural gas Location: open basement Heat Distribution: forced air

4. DOMESTIC HOT WATER HEATING:

Fuel: natural gas Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplace
Fuel: wood
Frequency of Use

Frequency of Use: once per week Chimney Type: insulated metal

6. EXHAUST FANS FREQUENTLY USED:

main bathroom central vacuum master bedroom bathroom

7. DOORS/WINDOWS FREQUENTLY USED:

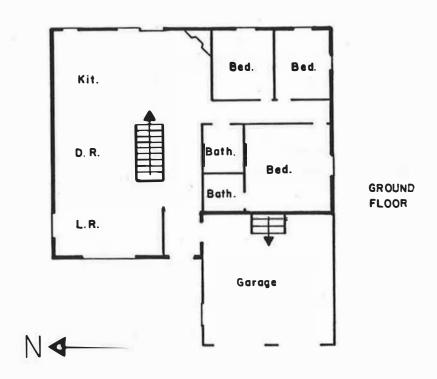
main entrance kitchen window basement door garage door

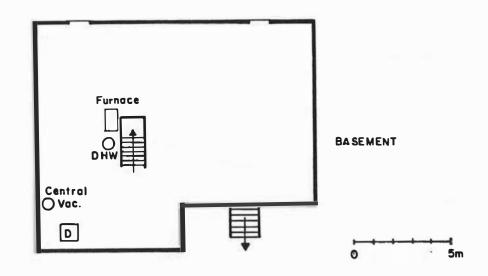
8. FAN TEST CHARACTERISTICS:

1.88 Air Changes per Hour (@ 50 Pa)
0.051 Equivalent Leakage Area (m²)

9. HOMEOWNER PROFILE:

Occupants 18 years and older: 2
Occupants under 18 years: 1
Number of occupants who smoke: 2





HOUSE W-3

Air Analysis Results of Residential Combustion Spillage Monitoring

T 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2													
		:gggrbbA	M3		C	ity: W	linnipeq	F	uel Typ	e: G	as		
SPILLAGE Type	Dațe	Location	GA: NO2 (ppm)	STEC Tut NOx (ppm)	902 (ppm)	CO (ppm)	CO2 (ppm)		H.C (ppm)	02	Sorben NO2 (ppm)	t Tubes ,NO (ppm)	Pump Time (sec.)
FRE SPILL	Mar 17	near furnace living room	0	0 0		1.9	669	3.1	2.7	21			
FORCED	Mar 17	near furnace living room	0	trace 0		1.1	1268	2.7	2.1	21			
POST SPILL	Mar 17	near furnace living room	0	0									

HOME PROFILE

- I. HOUSE IDENTIFICATION: No. W-4
- 2. HOUSE DESCRIPTION:

Total Floor Area: 237 m², one storey, single detached

3. SPACE HEATING:

Fuel: natural gas Heat Distribution: forced air location: enclosed furnace room

4. DOMESTIC HOT WATER HEATING:

Fuel: natural gas
Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplace Fuel: wood

Frequency of Use: twice per season

Chimney Type: masonry

6. EXHAUST FANS FREQUENTLY USED:

clothes dryer master bedroom bathroom main floor bathroom

7. DOORS/WINDOWS FREQUENTLY USED:

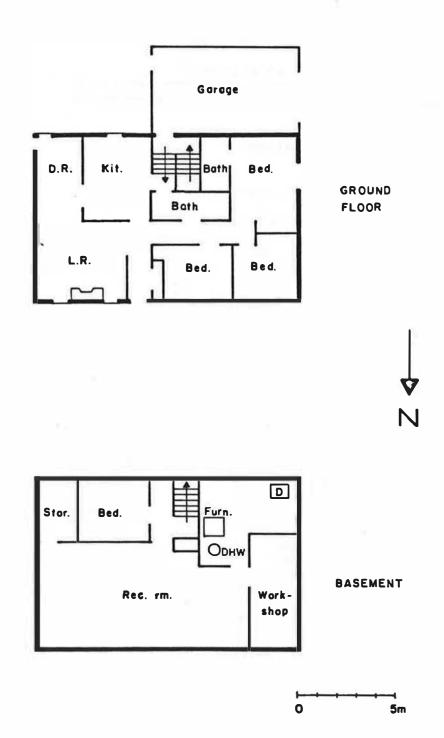
main entrance garage door workshop window

8. FAN TEST CHARACTERISTICS:

3.18 Air Changes per Hour (@ 50 Pa) 0.072 Equivalent Leakage Area (m²)

9. HOMEOWNER PROFILE:

Occupants 18 years and older: 4
Occupants under 18 years: 1
Number of occupants who smoke: 3



HOUSE W-4

Location Code: W 4

Start date: 18mar87 End date: 24mar87

Total Number of Days Analyzed in these Tables: 6

Total Number of Days Monitored for this House:19

TABLE1:FREQUENCY AND DURATION OF SPILLAGE EVENTS

Spillage time Interval	Total Sp	illage	Events
(sec)	Furnace	DHW T	otal
10-29	0	57	57
30-120	0	47	47
>120	0	59	59
Total	0	163	163

TABLE 2: AGGRAVATING CONDITIONS DURING SPILLAGE EVENTS

List of Fireplace	*		% Time Condition	Spillag	ge Events	Total Window Open
		Devices	True	Totals	Time(min)	Occurrences
OFF	OFF	OFF	84.743	71	604.88	23
OFF	ON	OFF	14.845	78	620.77	18
OFF	OFF	ON	0.411	14	36.15	3
OFF	ПO	ON	0.000	0	0.00	0
ON	OFF	OFF	0.000	0	0.00	0
OIA	ON	OFF	0.000	O	0.00	0
ON	OFF	ON	0.000	0	0.00	0
ON	ЫO	ON	0.000	0	0.00	О

TOTAL: 163 1262

note:column "% Time Condition True" has device status forced on if device is spilling

Location Code: W4
Start date: 01APR87 End date: 08APR87
Total Number of Days Analyzed in these Tables: 7
Total Number of Days Monitored for this House: 19

TABLE1: FREQUENCY AND DURATION OF SPILLAGE EVENTS

Sp	oillage time	Total Sp	illage Ev	ents.
	Interval			
a district	(sec)	Furnace	DHW Tot	al
	10-29	0	34	34
	30-120	0	32	32
•	>120	0	66	66
	Total	0.	132	132

TABLE 2:AGGRAVATING CONDITIONS DURING SPILLAGE EVENTS

List of (% Time Condition	Spilla	ae Events	Total Window Open
	jt	Devices	True	Totals	Time(min)	Occurrences
OFF	OFF	OFF	85.783	53	587.47	17
OFF	OΝ	OFF	13.691	72	708.15	29
OFF	OFF	OΝ	0.506	5	67.88	1
OFF	ИO	NO	0.017	2	56.10	2
OΝ	OFF	OFF	0.000	O	0.00	0
ио	אט	OFF	0.000	0	0.00	Q
0 N	OFF	ดห	0.003	0	0.00	0
OW	ИО	ОИ	0.000	0	0.00	0

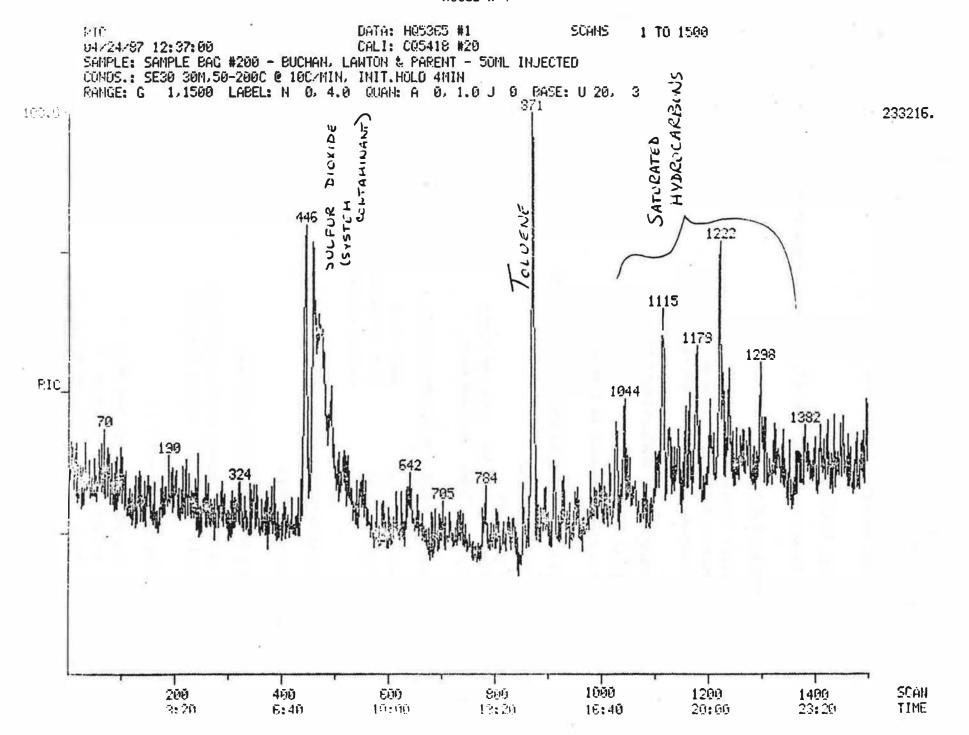
TOTAL: 132 1420

note:column "% Time Condition True" has device status forced on if device is spilling

Air Analysis Results of Residential Combustion Spillage Monitoring

		Address:	W4		C	ity: W	linnipeg	F	uel Typ	e:	Gas		
SPILLAGE			GAS	TEC Tub	25		1	Bag Samp	les		Sorbe	nt Tubes	Pump
	Date ~		NO2	NOx (ppm)	SO2	CO	C02	CH4	H.C	02	NO2	NO (ppm)	Time
PRE SPILL	Mar 18		0			0.5	919	2.1	1.2	21			
FORCED	Mar 18	near furnace kitchen		0		5.3	1998	2.9	1.4	21			
OST SPILL	Mar 18	near furnace kitchen	0	0									
CONTROLLED	Mar.31 -												
	Apr.1	near furnace				1	1118	1.7	3.3	21	0.012	0.094	10359
	Apr.1-2	•				0.5	1056	2	3.3		0.049		4595
	Apr.2-3	•				1.1	1361	2.3	1.8		0.057		8167
	Apr.3-4	•				0.5	520	3.8	1.6		0.056	0.264	952
	Apr.4-5	•				1.1	1215	2.3	1.6	21			
	Apr.5-6											0.269	1521
	Apr.6-7	•				1.1	1590	1.9	2	21			
	Aor.7-8					0.8	1383	1.7	1.5		0.076	0.159	953
	Apr.17-19	•	¥ M.S.¥			0.9	1342	1.8	9.9	21			
				A	G. –	0.88		2.2	3.1		0.053	0.227	
IMED	Mar.31 -												
	Aor.1	near furnace				0.5	655	2.4	2.7	21			1170
	Aor.1-2	•				1	695	2.3	3.8	21			45
	Apr.2-3	•				2.2	568	2.3	2.2	21			45
	Aor.3-4					0.8	772	2.3	1.9	21			39
	Apr.4-5					1.6	822	2.6	1.5	21			300
	Apr.5-6					1.1	735	3.6	2.4	21			15
	Apr.6-7					1.1	983	2.2	2.3	21			24
	Apr.7-8	•				0.8	824	1.9	1.5	21			27
					_								

NOTE: M.S. = MASS SPECTROMETER DONE.



HOME PROFILE

- I. HOUSE IDENTIFICATION: No. W-5
- 2. HOUSE DESCRIPTION:

Total Floor Area: 216 m², split-level, single detached

3. SPACE HEATING:

Fuel: natural gas
Heat Distribution: forced air
Location: enclosed furnace room

4. DOMESTIC HOT WATER HEATING:

Fuel: natural gas Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplace Fuel: wood

Frequency of Use: once per season Chimney Type: insulated metal

6. EXHAUST FANS FREQUENTLY USED:

main bathroom

range hood

clothes dryer

both upstairs bathrooms

central vacuum

7. DOORS/WINDOWS FREQUENTLY USED:

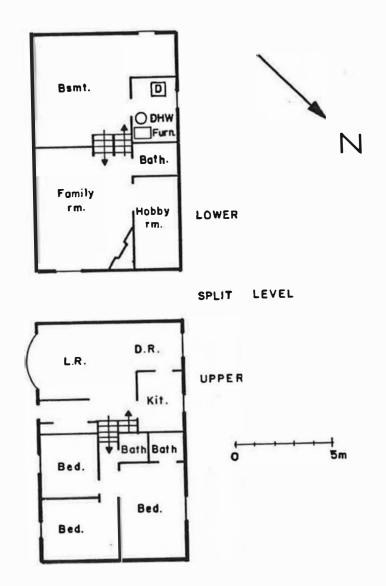
main entrance

8. FAN TEST CHARACTERISTICS:

1.83 Air Changes per Hour (@ 50 Pa) 0.034 Equivalent Leakage Area (m²)

9. HOMEOWNER PROFILE:

Occupants 18 years and older: 2
Occupants under 18 years: 2
Number of occupants who smoke: 0



HOUSE W-5

Air Analysis Results of Residential Combustion Spillage Monitoring

		Address:	N 5		С	ity: W	innipeq	F	el Type	e: G	as		
SPILLAGE			GA	STEC Tub	es		E	ag Samp	105		Sorbent	Tubes	Pump
TYPE	Date	Location	NO2 (ppm)	(ppm)	SO2 (ppm)	(ppm)	CO2 (ppm)	CH4 (ppm)	H.C (ppm)	02 (%)	NO2 (ppm)	NO (ppm)	Time (sec.)
PRE SPILL	Mar 19	near furnace	0	0		1.9	1249	2	2.1	21			
FORCED	Mar 19	living room near furnace living room	trace 0	0 7.5 trace		0.8	3568	1.5	2	21			
POST SPILL	Mar 19	near furnace living room	0	trace 0									

HOME PROFILE

- I. HOUSE IDENTIFICATION: No. W-6
- 2. HOUSE DESCRIPTION:

Total Floor Area: 235 m², single storey, single detached

3. SPACE HEATING:

Fuel: natural gas
Heat Distribution: forced air
Location: open basement

4. DOMESTIC HOT WATER HEATING:

Fuel: natural gas Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: none Fuel: n/a

Frequency of Use: n/a Chimney Type: n/a

6. EXHAUST FANS FREQUENTLY USED:

main bathroom clothes dryer master bedroom bathroom

7. DOORS/WINDOWS FREQUENTLY USED:

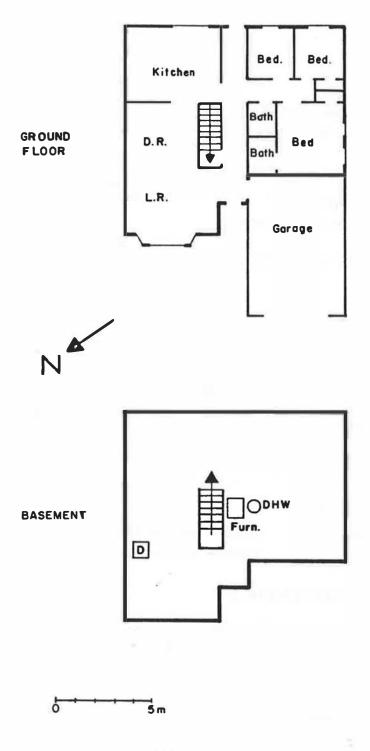
main entrance living room window garage door kitchen window

8. FAN TEST CHARACTERISTICS:

1.95 Air Changes per Hour (@ 50 Pa)0.041 Equivalent Leakage Area (m²)

9. HOMEOWNER PROFILE:

Occupants 18 years and older: 2
Occupants under 18 years: 1
Number of occupants who smoke: 2



HOUSE W-6

Air Analysis Results of Residential Combustion Spillage Monitoring

		Address: N	16		C	ity: W	innipeg	F	uel Typ	e: G	 35		
SPILLAGE TYPE	Date.	Location	GAS NO2 (ppm)	TEC Tub NOx (ppm)	965~ \$02 (ppm)	CO (ppm)	B CO2 (ppm)	ag Samp CH4 (ppm))les~ H.C (ppm)	02	Sorbent NO2 (ppm)	Tubes NO (ppm)	Pump Time (sec.)
PRE SPILL	Mar 20	near furnace living room	. 0	0									
FORCED	Mar 20	near furnace living room	0.2	2.5		3.6	2592	3.3	2	21			
POST SPILL	Mar 20	near furnace living room	0	0									

HOME PROFILE

- I. HOUSE IDENTIFICATION: No. W-7
- 2. HOUSE DESCRIPTION:

Total Floor Area: 213 m², two storey, single detached

3. SPACE HEATING:

Fuel: natural gas
Heat Distribution: for

Heat Distribution: forced air Location: enclosed furnace room

4. DOMESTIC HOT WATER HEATING:

Fuel: natural gas

Location: adjacent to furnace

5. SUPPLEMENTARY COMBUSTION SYSTEMS:

Type: fireplace

Fuel: wood

Frequency of Use: once per winter month

Chimney Type: insulated metal

6. EXHAUST FANS FREQUENTLY USED:

clothes dryer

7. DOORS/WINDOWS FREQUENTLY USED:

main entrance

kitchen door kitchen window

garage door kitchen v

side door

8. FAN TEST CHARACTERISTICS:

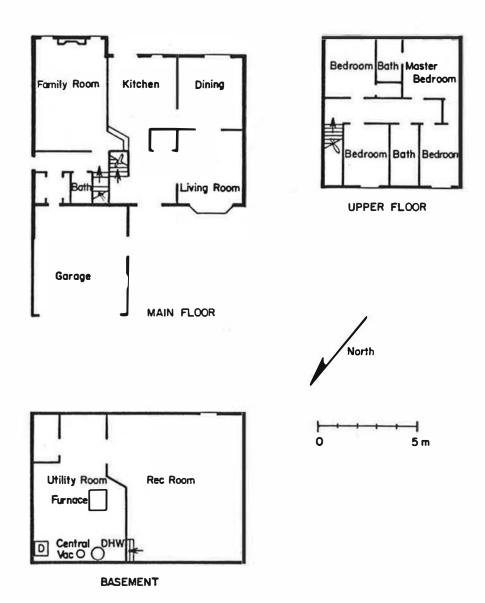
2.34 Air Changes per Hour (@ 50 Pa) 0.062 Equivalent Leakage Area (m²)

9. HOMEOWNER PROFILE:

Occupants 18 years and older: 2

Occupants under 18 years: 3

Number of occupants who smoke: 2



Air Analysis Results of Residential Combustion Spillage Monitoring

		Address: W	7		C	ity: W	innipeg	F	uel Tyo	e: G	35		
SP ILLAGE		Location	GASTEC Tubes			Bag Samp			oles		Sorbent Tubes		Pump
TYPE	Date		NO2 (ppm)	NO×	SO2 (ppm)	CO	C02	CH4	H.C (ppm)	02	NO2 (ppm)	NO (ppm)	Time (sec.)
PRE SPILL	Mar 22	near furnace	^	^									
LKE SLIFF	nar 22	living room	0	0									
FORCED	Mar 22	near furnace living room		trace trace		1.1	2567	3.2	1.5	21			
POST SPILL	Mar 22	near furnace -	0	0									
CONTROLLED	Mar.31 - Apr.1	At furnace				1	535	3.8	2.7	21			198
	uhiei	un Iniliace				1	333	J.0	ů = /	ů I			170
TIMED	Mar.31 - Apr.1	At furnace				0.5	473	4.1	3.5	21			540

APPENDIX B Mann Testing Laboratories Report





MANN TESTING LABORATORIES LTD. 5550 McADAM ROAD, MISSISSAUGA, ONTARIO L4Z 1P1 PHONE: 890-2555 • TELEX: 06-960496

June 15, 1987

Buchan, Lawton & Parent Ltd. 5370 Canotek Road Ottawa, Ontario K1J 8X7

Attention: Mr. Mark Lawton

RE: MASS SPECTROMETER INFORMATION

In response to your telephone call of June 5th, 1987, I am pleased to submit the following information to assist you with the interpretation of your project results.

There are limitations inherent in both the method of sampling and the mass spectrometer itself. The mass spectrometer has a lower detection limit of low to sub ppb and detects only compounds with a molecular weight greater than 40. The use of the bag sample technique limits the analytical detectability to volatile organics.

All of the samples submitted for GC/MS qualitative screening were analyzed for total volatile hydrocarbon and found to be under 10 ppm methane equivalents; with samples #22 and #34 under 2 ppm methane equivalents. As an example, if 1 ppm of toluene (C_7H_8) was present it would translate approximately to 7 ppm methane equilvalents (i.e. toluene 7 carbons to methane 1 carbon).

The samples, therefore all contain ppb levels of the compounds found.

If you have any further questions please contact either Betsy Cliffe or myself.

Yours truly,

MANN TESTING LABORATORIES LTD.

W.R. Burgess, B.Sc., C. Chem. Manager, Occupational Health

al a way both

WRB/vs



MANN TESTING LABORATORIES LTD. 5550 McADAM ROAD, MISSISSAUGA, ONTARIO L4Z 1P1 PHONE: 890-2555 • TELEX: 06-960496

April 23, 1987

Buchan, Lawton & Parent Ltd. 5370 Canotek Road Ottawa, Ontario K1J 8X7

Attention: Mr. Mark Lawton

RE: MANN TESTING FILES 876723/876728

MASS SPECTROMETER RESULTS

BAG SAMPLES 22/34

Dear Mr. Lawton:

Your two bag samples were analyzed by Gas Chromatography/Mass Spectrometer (GC/MS) under the following conditions:

Injection Volume: 50 mL
Initial Temperature: 50°C
Initial Hold Time: 4 min.
Final Temperature: 200°C
Temperature Ramp: 10°C/min
Column: 30M, SE30

The samples were analyzed using a Universal Automated Concentrator Instrument Model 780, which passes the released organics through two sorbent traps of large and small bore. The latter trap serves to reduce the sample to a small concentrated plug prior to its separation with a 30 meter Superox GC capillary column, and subsequent analysis by a Finnigan Model 3200 Mass Spectrometer.

RECEIVED APR 2 8 1987

The data thus produced are stored in the memory of the computer and matched with the spectra from the United States Environmental Protection Agency/National Institute of Health library, which contains mass spectra of over 40,000 compounds.

The enclosed GC/MS chromatograms have been labelled with the compounds found in the respective samples. The most abundant compounds are saturated hydrocarbons which are aliphatic straight chained hydrocarbons (e.g. C_xH_{2x+2}).

If you have any questions concerning this data, please contact Betsy Cliffe or myself.

Yours truly,

MANN TESTING LABORATORIES LTD.

W.R. Burgess, B.Sc., C.Chem. Manager, Occupational Health

WRB/jh, Encl.



MANN TESTING LABORATORIES LTD. 5550 McADAM ROAD, MISSISSAUGA, ONTARIO L4Z 1P1 PHONE: 890-2555 • TELEX: 06-960496

May 4, 1987

Buchan, Lawton & Parent Ltd. 5370 Canotek Road Ottawa, Ontario K1J 8X7

Attention: Mr. Mark Lawton

RE: MANN TESTING FILE NO. 876954 MASS SPECTROMETER RESULTS SAMPLE BAG NO. 200

Dear Mr. Lawton:

Your bag sample was analyzed by Gas Chromatography/Mass Spectrometer (GC/MS) under the following conditions:

Injection Volume: 50 mL
Initial Temperature: 50°C
Initial Hold Time: 4 min.
Final Temperature: 200°C
Temperature Ramp: 10°C/min
Column: 30M, SE30

The sample was analyzed using a Universal Automated Concentrator Instrument Model 780, which passes the released organics through two sorbent traps of large and small bore. The latter trap serves to reduce the sample to a small concentrated plug prior to its separation with a 30 meter Superox GC capillary column, and subsequent analysis by a Finnigan Model 3200 Mass Spectrometer.

The data thus produced are stored in the memory of the computer and matched with the spectra from the United States Environmental Protection Agency/National Institute of Health library, which contains mass spectra of over 40,000 compounds.

The enclosed GC/MS chromatogram has been labelled with the compounds found in the sample. The most abundant compounds are saturated hydrocarbons which are aliphatic straight chained hydrocarbons (e.g. C_xH_{2x+2}).

If you have any questions concerning this data, please contact Betsy Cliffe or myself.

Yours truly,

MANN TESTING LABORATORIES LTD.

W.R. Burgess. B.Sc..(

W.R. Burgess, B.Sc., C.Chem. Manager, Occupational Health

WRB/bc, Encl.

APPENDIX C Tracer Gas Sampler Analysis



General Description of the NAHB Research Foundation/ AIMS Output Format

June 1987

The top portion of the sheet shows the project title, house identification, start and stop times and dates for sampling, final date that computations were made, and date of the analysis.

The Rates Section gives the overall infiltration rate in cubic meters per hour (m /hr) for all zones, and the air change rate per hour (ACH), obtained by dividing the air infiltration rate by the total volume. For each zone, the zone location, source information (gravimetric calibration rate at 25 degrees C., quantity, total emission rate adjusted for temperature, assuming an enthalpy of 6.8 kcal/mole), and exfiltration and infiltration rates with their standard deviations (SD's) are given, followed by the zone-to-zone air flow rates and SDs, and total flow in or out of each zone.

The <u>Analysis Section</u> gives, for each zone, the volume, source type, and average tracer concentration with SD's, followed by the individual capillary absorption tracer (CATS) analyses by zone with correction factors.

The <u>Notes Section</u> gives the SD's assigned to the source rates and volumes. Conditions or results that should not exist are flagged by printing in capital letters.

The current PFT tracer codes are:

Type	Tracer Name	Abbreviation
1	Perfluorodimethylcyclobutane	PDCB
8	Perfluoromethylcyclopentane	PMCP
2	Perfluoromethylcyclohexane	PMCH
3	Perfluorodimethylcyclohexane	PDCH

NAHB-RESEARCH FOUNDATION OF AIMS

07-01-1987 START: 18:00 (02-26-1987) STOP: 15:00 (03-16-1987) PROJECT: RES COMB.S FILE: 1BUCH HOUSE: 02 ANALYZED: 06-30-1987 OVERALL INFILTRATION RATE = OVERALL AIR EXCHANGE RATE = 133.6 ± 12.7(m³/h) 0.263 ± 0.027(1/h) ZONE SOUR LOCATION @25C (nL/m) UPPER ZONE 35.9 BASEMENT 24.7 EXFILTRATION RATE S --INFILTRATION-SOURCE RATE ACH (/h) LOCATION RATE SD SD QTY 88.9 SD (nL/h) 3272 2253 (m^3/h) E 0.073 85.4 48.2 13.5 0.440 16.6 44.7 2 BASEMENT 8.3 0.02711.2 0.153ZONE-ZONE RATE $SD (m^3/h)$ ZONE-ZONE RATE $SD (m^3/h)$ 7.5 TOTAL FLOW IN OR OUT-± SD(/h) ZONE RAT ZONE ACH ± SD(/h) RATE \pm SD (m³/h) RATE \pm SD (m^3/h) ACH ± SD(/h) 18.9 0.6320.102 \mathbb{Z} 81.9 12.6 0.261*********************************** ANALYSIS ********************* Z VOL SOURCE AVG. TRACER CONC N (p! /L) ± SD PMCP 30.49 ± PMCH 9.54 ± 31.45 ± E 194 EMICE 314 EMICH 0.95 3.05 12.54 ± 1.25 3.14 CATS# CONCENTRATION (pL/L) PMCF PMCH PDCB PDCH 30.492 12.542 9.539 1.447 0.202 0.237.: PDCB **EMCP** FMCH FDCH COEFFICIENTS FILE 0.97 0.89 0.97 0.89 SAIMPERA **************** ****** NOTES

The standard deviation in the source strength has been set at $10\ \%$. The standard deviation in the volume measurement has been set at $5\ \%$.

NAHB-RESEARCH FOUNDATION 07-01-1457

PROJECT: RES COMB.S HOUSE: 03 START: 10:00 (03-06-1987) STOP: 15:30 (03-16-1987) 18UCH 06-30-1987 ANALYZED: 108.3 ± 15.0(m³/h) 0.239 ± 0.034(1/h) OVERALL INFILTRATION RATE = OVERALL AIR EXCHANGE RATE = SOURCE RATE @25C OTY @ ZONE EXFILTRATION ---INFILTRATION--RATE е́т RATE (m^3/h) -11.9 120.3 (/h) -0.053 0.123 0.531 0.133 (nL/m) 35.9 24.7 (nL/h) 3272 2253 (m^3/h) Ε 27.8 29.5 66.5 41.9 25.6 36.6 BASEMENT ZONE-ZONE i - 2 RATE 105.3 ZONE-ZONE $SD (m^3/h)$ RATE 183.7 ± $SD (m^3/h)$ ± 58.6 171.7 48.5 0.759 2 225.5 0.217 0.996 0.285 63.7 ********************************** ANALYSIS *********************** VOL SOURCE AVG. TRACER CONC. KE PMCH PMCP 2.13 2.00 38.05 ± 17.76 ± 21.34 ± 19.95 ± 226 PMCP 225 PMCH CATS# CONCENTRATION (pL/L) PDCH PMCP F'MCH PDCB 117 - 8.049 161 - 17.761 21.338 19.952 0.033 0.058 0.043 COEFFICIENTS FILE SAIM2FMA PMCH PMCH PDCH 0.57 0.57 C.F.: FDGB 0,29

The standard deviation in the source strength has been set at 10%. The standard deviation in the volume measurement has been set at 5%. COP 19 LESS THAN COP ... THE NORTH IS NEGATIVE

NAHB-RESEARCH FOUNDATION AIMS

07-02-1987 PROJECT: 2332 START: 17:00 (03-09-1987) STOP: 12:10 (03-26-1987) 1 BUCH HOUSE: 05 06-30-1987 ANALYZED: *********** RATES ******************** 74.2 0.010 OVERALL INFILTRATION RATE = OVERALL AIR EXCHANGE RATE = ± 10.4(m^3/h) ± 0.001(1/h) SOURCE RATE @25C DTY @ (nL/m) (nl ZONE EXFILTRATION !----INFILTRATIONeT RATE (m^3/h) ACH LOCATION RATE SD (m^3/h) SD (**/h)** (nL/h) 3272 2253 0.002 0.001 10.4 73.6 10.5 35.9 24.7 73.7 BASEMENT 0.6 0.10.6 0.10.004 ZONE-ZONE $SD (m^3/h)$ ZOIVE-ZONE RATE RATE SD (m^3/h) 0.1---TOTAL FLOW IN OR OUT-----ACH ± SD(m^3/h) RATE ± SD (m^3/h) ACH ± SD(/h) ACH ± SD(/h) 74.1 10.5 0.010 0.002 0.1 0.007 0.000 1.0 AVG.TRACER CONC. (pL/L) ± SD-VOL SOURCE ō 12C m^{-3} PMCH PMCP 7224 PMOR 151 FMOR 4.43 12.33 ± 1.23 1.87 2249.29 ± %224.93 44.29 ± 18.72 ± CATS# CONCENTRATION (PL/L) PMCP **PMCH** PDCB PDCH 44.2**8**5 12.326 18.72**0**2249.289 465 PMCH O.97 COEFFICIENTS FILE 361M2FMA FDLB 0.89 0.5990.97 Ine standard deviation in the source strength has been set at 10.7 . The standard deviation in the volume measurement has been set at ± 2.7 Impurities found on tabe # 465 (Space Room)

and this caused the ACH 0.010 to be low and may to not be reliable. The actual ACH Low

this house should be higher than 0.010.

NAHB-RESEARCH FOUNDATION

07-02-1987 FROJECT: 2832 HOUSE: 06 START: 10:00 (03-19-1987) STOP: 11:30 (03-27-1987) 18UCH 06-30-1987 ANALYZED: OVERALL INFILTRATION RATE = OVERALL AIR EXCHANGE RATE = 318.4 0.688 28.5(m/3/h) ± 0.066(1/h) SOURCE RATE @25C QTY @ (nL/m) (nL. 35.9 2 32 24.7 2 22 EXFILTRATION RATE SI :----INFILTRATION-(m^3/h)
221.7 58.8
96.7 58.8 ēт (m^3/h) 161.3 157.1 LOCATION ACH (nL/h) 38.6 33.5 (/h) 0.576 0.141 0.862 0.189 BOYS BED 1 BOYS BED 2 BASEMENT **RATE** 192.2 ZONE-ZONE 2 - 1 RATE 252.7 SD (m^3/h) ZONE~ZONE $SD (m^3/h)$ **±** ± 54.6 1.477 70.2 1.916 - 0.357 414.0 83.1 0.306 349.3 Z 0 VOL SOURCE AVG. TRACER CONC. NE (pL/L) ± SD--FMCF FMCH THE PHEH 11.90 ± 6.55 ± 5, 93 ± 9,71 ± 1.15 0.59 0.35 5.7 CATS# CONCENTRATION (PL/L) PMCP PMCH PDCB PDCH 5. 727 7.1 11.901 6.549 0.078 O, OO 0.000 FLCB FMCF FMCH 0.85 0.87 0.97 COEFFICIENTS Foun 0.89 0.89 0.97 0.57 SAIM2FMA

The scandard deviation in the source strength has been set at $\pm 0.5\%$. The standard deviation in the volume measurement has been set at $\pm 5.5\%$

NAHE-RESEARCH FOUNDATION AIMS 07-01-1967 PROJECT: RES COMP.S START: 13:30 (03-10-1987) STOP: 14:00 (03-27-1987) 18UCH 06-30-1967 FILE: ANALYZED: OVERALL INFILTRATION RATE = OVERALL AIR EXCHANGE RATE = 210.0 22.3(m/3/h) 0.449 $\pm 0.050(1/h)$ EXFILTRATION RATE SI -INFILTRATION-SOURCE RATE SD RATE ēт SD ACH (m^3/h) 52.8 57.0 (m^3/h) (/h) (nL/h)15.8 $\frac{10.1}{25.1}$ 0.226 0.045 $3\overline{2}72$ 2253157.2 174.B 0.11231.2 $SD (m^3/h)$ $SD (m^3/h)$ ZONE-ZONE RATE RATE ± 11.5 **68.4** 50.6 ---TOTAL FLOW IN OR OUT-CH ± SD(/h) ZONE RA RATE ± SD (m^3/h) RATE \pm SD (m^3/h) ACH ± SD(/h) ACH ± SD(/h)

225.6

CONCENTRATION (pL/L)

35.5

0.964

************************************ ANALYSIS ********************* AVG. TRACER VOL SOURCE ō NE m^3 $-(pL/L) \pm SD-$ PMCH 5.75 ± 11.73 ± PMCP 234 PMCP 234 PMCH 37.12 ± 11.25 ± 1.13

0.073

PMCP PMCH PDCB PDCH 37.115 11.250 . 754 0.000 0.000

0.443

HÜUSE:

ZONE

LOCATION

BASEMENT

ZONE-ZONE

ZONE

HALL

07

CATS#

@25C (nL/m) 35.9 24.7

FHCF PDCH COEFFICIENTS FILE C.F.: FUCB 0.570.970.69 0.89

10 %. at E %. The standard deviation in the source strength has been set at 19. The standard deviation in the volume measurement has been set at

NAHB-RESEARCH FOUNDATION
07-02-1987

PROJECT: 233 START: 15:00 (03-31-1987) STOP: 18:00 (04-19-1987) FILE: 1BUCH HOUSE: 06-30-1987 ANALYZED: OVERALL INFILTRATION RATE = OVERALL AIR EXCHANGE RATE = ± 26.5(m^3/h) ± 0.048(1/h) 218.4 0.378 RATE EXFILTRATION RATE ZONE SOURCE RATE @25C QTY LOCATION @T SD ACH (nE/h) 2440 (m^3/h) (m^3/h) 189.3 29.1 (/h) 45.0 24.2 34.5 13.9 0.655 BASEMENT 24.7 MASTER BED 35.9 0.124204.1 12.3 3544 0.101 0.048 ZONE-ZONE 2 - 1 RATE ± ZONE-ZONE RATE SD SD (m^3/h) ± (m^3/h) 28.0 32.6 1 - 2 103.3 120.1 ----TOTAL FLOW IN OR OUT--ACH ± SD(/h) ZONE RATE ZONE RATE \pm SD (m^3/h) RATE ± SD (m^3/h) ACH ± SD(/h) 309.4 58.9 1.071 25.2 0.458 0.211 132.5 0.090 ******************************** ANALYSIS ******************* Z VOL SOURCE AVG. TRACER CONC. /L) ± SD NE - (pl PMCP PMCH 285 PMCH 289 PMCP 11.31 ± 8.82 ± 1.13 14.90 ± 38.37 ± 0.88 5.84 CATS# CONCENTRATION (pL/L) PMCH. PMCP PDCB P'DCH ÷. 14.899 0.077 0.049 Q. Q7 OLUKA) 0.000 РМСР U.39 PMCH 0.97 $PD(_{\alpha}B$ PDCH COEFFICIENTS FILE 0.97 SATH2FMG 0.89 ********* NOTES The standard deviation in the source strength has been set at ± 0.00 fine standard deviation in the volume measurement has been set at

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. /05_7:_1.1007) ETLT: 100Fb

PROJECT: 233 HOUSE: W START: 12:00 (03-31-1987) STOP: 18:00 (04-16-1987) 1BUCH 06-30-1987 ANALYZED: OVERALL INFILTRATION RATE = OVERALL AIR EXCHANGE RATE = ± 12.3(m⁴ ± 0.034(1/h) 12.3(m^3/h) SOURCE RATE @25C OTY @ (nL/m) (nL EXFILTRATION !----INFILTRATION-RATE (m^3/h) RÂTÊ (m^3/h) SD ēт LOCATION ACH (nL/h) (/h) 0.644 0.105 0.171 0.030 **`3/h)** 15.7 10.2 1 BASEMENT 24.7 2 MASTER BED 35.9 2440 3544 I BASEMENT 42.4 44.6 RATE 30.5 SD (m^3/h) ZONE-ZONE SD (m^3/h) ZONE-ZONE RATE 6.7 ACH ± SD(/h) ZONE RATE ± SD (m^3/h) ACH ± SD(/h) ZONE RATE \pm SD (m^3/h) ACH \pm SD(/h) 17.7 75.1 0.289 0.8950.144 11.4 116.4 ********************************** ANALYSIS ******************* VOL SOURCE AVG. TRACER ō CONC. -(pL/L) ± SD-N PMCP Ξ PMCH 130 PMCP 280 PMCP 73.60 ± 14.05 ± CONCENTRATION (pL/L) CATS# F:MCH PMCP PDCB 14.947 55.272 lulagi 0.210 0.000 0.084 0.000 C.F.: PPCB AMCR FMCH 0.89 0.97

the standard deviation in the source strength has been set at 10 %. The standard deviation in the volume measurement has been set at 2 %

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07-02-1987 START: 17:40 (03-30-1987) STOP: 16:00 (04-16-1987) PROJECT: 2332 FILE: TRUCH 06-30-19B7 ANALYZED: HOUSE: OVERALL INFILTRATION RATE = OVERALL AIR EXCHANGE RATE = 143.9 0.229 ± . 16.5(m^3/h) ± 0.028(1/h) ZONE SOURCE RATE (m^3/h)
117.2
26.7 **EXFILTRATION** -INFILTRATION--LOCATION @25C OTY (nL/m)
BASEMENT 35.5 2
MASTER BED 24.7 2 @T SD RATE ACH (m^3/h) 119.5 23.6 (nL/h) 3544 (/h) 0.588 18. E 17.6 0.091 3544 2440 4.4 0.011 6.0 0.057 ZONE-ZONE SD RATE ZONE-ZONE SD (m^3/h) RATE (m^3/h) ----TOTAL FLOW IN OR OUT-ACH ± SD(/h) ZONE RATE ŻONE $RATE \pm SD (m^3/h)$ RATE \pm SD (m^3/h) ACH ± SD(/h) 20.2 0.675 44.4. 0.1050.104 U. 010 Z VOL SOURCE AVG. TRACER CONC. KE (PL PMCH PMCP 24.14 1941.6 27.36 ± 1 1. 121-14 1.26 CONCENTRATION (pL/L) P'MCF **FMCH** F-DCB PDCH 0.082 FDLR G.SF $\vdash [v] \bigcap_{i=0}^n$ FINDH COEFFICIENTS FILE 0.97 0.89 3AIMEMA 0.97 ine standard deviation in the source strength has been set at

The standard deviation in the volume measurement has been set at

