# EFFECTS OF NON-ISOTHERMAL AND INTERMITTENT AIR MOVEMENT ON HUMAN THERMAL RESPONSES

Zhao Rong-yi, Xia Yi-zai

**AIVC 12094** 

Dept. of Thermal Engineering, Tsinghua University, Beijin

#### **ABSTRACT**

Twenty-four college students are asked about their subjective responses to a dynamic thermal environment with nonisothermal and intermittent air movement. The subjects wear an uniform of 0.6 clo and A rotative air jet can are sedentary. cyclically sweep over the subjects with adjustable air velocity. Each experiment lasts 150 minutes and is performed with three stages. Changing pattern of TSV and TCV over time, the effects of the frequency of the rotative jet on human's thermal sensation and thermal comfort, and the relation between the rotative frequency of the air jet and the velocity sensed by the subjects are studied. Non-isothermal and intermittent cool jet improves the subjects' conditions significantly increased their acceptance of the thermal environment. The subjects respond immediately to the temperature step-change, and as time passes by, the sensitivity to the cool air is diminishing. The sensed velocities are variable at different rotative speeds of the outlet. Under different air temperature conditions, the preferred speed of rotation is varied.

## **KEYWORDS**

thermal comfort, air movement, intermittent, non-isothermal

# INTRODUCTION

To provide a healthy and acceptable thermal environment with minimized energy consumption and environment pollution is valuable for developing countries, especially for those located in tropic and subtropic areas. Although the use of air conditioning could improve the indoor climate by maintaining the room temperature lower(e.g. 24°C--26°C), more complaints come from "non-adaptability of air conditioning". For this reason, a series of experimental studies on human responses to higher room air temperature with non-isothermal intermittent air movement has conducted.

Air movement is one of the main affecting human thermal responses. Air movement can provide thermal comfort and freshness in hot conditions. At environmental temperatures up to 30°C, the heat balance of the human body can be maintained efficiently by an increased heat loss caused by forced with isothermal convection airflow. Experiments performed by Burton et al. (1975), Rohles et al. (1983) and Scheatzle et al. (1989) showed that a ceiling fan providing air movement with a velocity up to 1 m/s may extend the upper limit of the summer comfort zone from 26°C to 29°C.

When the temperature of indoor environment is higher than 30°C, a reduction of heat stress can be achieved by cool air jets. Some experiments made by Azer and Nevins (1974), Melikov et al (1994) showed that the convective spot-cooling can decrease the physiological and subjective thermal stresses of the subjects participating in the experiments and increase the acceptability of the thermal environment. These studies provided useful information about the effect of local cooling by a "still" air jet at room air temperatures of more than 30°C. But what's the human responses when their whole bodies are exposed to the cool air provided by a rotative air jet, which creates a dynamic velocity and temperature fields? In the present study, some experiments are carried out to investigate the effects of this kind of non-isothermal and intermittent air jet to the thermal sensation and thermal acceptance of the. subjects.

The experiments contain the following aspects:

- 1. the transient and mean thermal sensation and thermal comfort over time.
- 2. the effects of the frequency of the rotative jet on human's thermal sensation and thermal comfort.
- 3. the relation between the rotative frequency of the air jet and the velocity

.

sensed by the subjects.

#### **METHOD**

#### **Experimental Facilities**

Climatic Chamber: The experiments are conducted in an environmental chamber with dimensions of 3.4m by 4.8m by 3m at Tsinghua University. The air is supplied uniformly from the ceiling with a velocity of less than 0.1m/s. The wall temperature is very close to the room air temperature.

Cooling System: An air conditioning unit with heater and cooler is installed to provide the cool air having a certain temperature. A rotary cylindroid terminal with a slotted outlet (width=20) is specially designed to generate the air jet different from the room temperature. The cool air is supplied to the terminal which is drived by an electric motor so that rotative speed could be changed. Therefore, a dynamic temperature and velocity field changed

cyclically with the rotative speed of the terminal is then created.

Measurement: The measuring and control system of the climatic chamber is based on the thermal resistance sensors for measuring temperatures of the room air and the six wall surfaces. These data are logged by a data acquisition unit at one-minute intervals. The characteristics of the cooling jets and air flow over the subjects are measured by thermal couples and hotbulb anemometer. The data are logged at 0.5 second interval and stored in a computer.

## Subjects and Clothing

24 college students of Tsinghua University are asked to be the subjects and paid for participating. Each subject is exposed to only one thermal environment for two hours. The anthropometric data for the subjects are listed in table 1.

Table 1 Anthropometric data for the subjects

	1 4010 1	. a.da opomio	TITO COCCOO TC.I OTT	- 5000	
Sex	Number of	Age	Height	Weight	Du Bois Area
	subjects	(year)	(m)	(kg)	$(\mathbf{m}^2)$
Females	4	19.89±0.76	1.61±0.06	53.50±5.23	1.55±0.05
Males	20	19.44±0.89	$1.69 \pm 0.05$	58.22±6.65	$1.66 \pm 0.11$
Females and Males	24	19.50±0.86	$1.68 \pm 0.06$	57.69 ± 6.43	1.65 ± 0.10

The subjects are instructed to arrive at the climate chamber wearing shoes, socks, trousers, underwear and long-sleeved shirt. For this ensemble, the thermal insulation is about 0.6 clo. During all experiments, the subjects are sedentary. They can chat and do some reading but cannot stand up and walk around.

#### **Experimental Procedure**

All experiments were done in November and December, 1997. The subjects reported 5 minutes prior to commencing the experiment, and it is ascertained that they do not feel sick. They change clothes for the hot environment for about half an hour in the climate chamber where the air temperature is 32.5°C. At the same time, they are trained the subjective rating scales and the experimental procedure.

Two subjects are arranged to take part in the experiment at the same time. They sit with broadside opposite to the outlet. The distances between the two subjects and the outlet are 0.7m and 1m respectively.

Every experiment is divided into three stages. In the first stage, every other 13 minutes, subjects are asked to write down on the questionnaire their "mean votes" of thermal sensation and thermal comfort which indicate subjects' general evaluation to the thermal environment with non-isothermal and intermittent air movement. Then they are asked to trace their "transient feelings" of thermal sensation and thermal comfort during the two periods of the terminal's rotation. At the end of this stage, the subjects fill in the table in the questionnaire (Fig 1).

In the second stage, the rotative speed of the outlet is changed by a litter knob beside the subjects. The rotary speeds were 3.4 rpm, 4.8 rpm, 6.8 rpm and 10.9 rpm respectively. At each speed, the subjects write down the "mean votes" of thermal sensation and thermal comfort, then plot out their transient feeling —thermal sensation vote (TSV) and thermal comfort vote (TCV)—versus time.

Because the different rotative speed of

the outlet will cause the different "sweeping time" of the air jet upon the human body, the mean velocity sensed by the subjects will also be different. As the limitation of the measuring instrument, it is unable to measure the changing velocity field at the position the subjects sit precisely. So in this experiment, the description of the velocity is based on that sensed by the subjects, and a "sensed velocity" is defined. When the maximum velocity sensed by the subjects while the outlet is rotating is almost

equal to the one sensed by the subjects while the outlet is standstill towards the subjects, the latter velocity is measured and regarded as the "sensed velocity" when the outlet is rotating at a certain speed. This is done in the third stage of the experiment.

Fig.1 shows the questionnaire including rating scales used by the subjects during the experiment.

1.55721170

Fig.,1 Questionnaire for subjective survey of thermal environment (every 13 minutes)

	OII VII OIIIIIOIII (	overy 15 minutes)				
Rating scale of thermal sensation and thermal comfort						
TSV	2 1	II TCV the state grade of				
2 3 25 : +3 1 . 240	hot.	*F 4 4 4 4 5 1 2 1 2 1 3 1 4 (200,00)				
ordina +2 .a caio:	warm	comfortable				
134 +1 mil 230 1	slightly warm	slightly uncomfortable age.				
a 0. 9 11	neutral	1 2 uncomfortable				
1 -1 5 % ·	slight cool	3 very uncomfortable do				
-2	cool	4 intolerable				
-3	cold					

Vote for the mean TSV and TCV and plot out your transient feelings of thermal sensation and thermal comfort during two periods of the terminal's rotation.

Fill in the table to assess the thermal environment.

Can you accept this thermal environment?  yes on no	what do you think of the temperature of cool air? ok or high or low	What do you think of the velocity of the jet? ok or high or low		
The Francisco to the part of	29 25 11 12	i ar and second		

. 21

#### RESULTS

15 fr ,

Table 2 lists the experimental conditions in the first stage of the experiment. Fig.2 and 3 show the transient TSV during the two rotative periods of the outlet at different testing time. subjects respond to the temperature stepchange quickly when they are exposed to the cool air... However, when the cool air leaves the subjects, the values of TSV rise slowly to the maximum as the cool air is about to come again. Furthermore, with the time goes on, the maximum of TSV corresponding with the time will decrease in different time period, while the minimum of TSV does not evidently change. So the change of difference between the maximum and minimum of TSV could be explained by of the adaptation of the subjects to this kind of uthermal environment. The longer the subjects are exposed to the intermittent cool air, the smaller the TSV difference is, and the more satisfactory the subjects feel. िराज्य इस ताल तीना अंधा ता कारताराष्ट्र हो न्या

Table		l conditions					
Exposure t	ime 80 mir	nutes, , ,					
Clothing	0.6 clo	141					
Activity	1 met	1 met ( sedentary.)					
Mean radia	nnt =Air to	=Air temperature					
temperatur		Co Harr					
	Condition A	Condition B					
Ta(°C)	· ~ 32	32.5					
Ti (°C)	B. 21.2	21.2					
L (m)		0.7					
Tjt (°C)	29.4	29.5					
F (rpm)	4.8	4.8					
Vjt (m/s)		1.7 En Tocs					
Vs (m/s)	0.81	0.91					
STRUME OF	44.	No. 1 1000					

ratio is gradually increased from 15 minutes to 80 minutes, and the cool effect is reducing with the time goes by

CONTRACTOR

In Fig. 5, the mean TSV has been plotted as a function of time. It can be seen that the TSV values tend to be constant after 67 minutes in two conditions. After 80 minutes, the mean general TSV seems to be constant(A-- 0.54; B--0.57), which shows that non-isothermal and intermittent cool air can improve the subjects' thermal conditions significantly and increases their acceptance of the thermal environment.

The change of TCV values connects with TSV tightly. When the least value of TSV is greater than zero, the minimum of TCV will appear at the moment the subjects are exposed to the cool air. But when the least value of TSV is smaller than zero, it is deemed that the most comfortable moment will appear at 2 seconds after being swept when TSV value is between 0 and 0.3.

Fig. 6 and 7 show the relationship between TSV and the rotative speed of the outlet in two periods in two experimental conditions. With the increase of the frequency, the effect of the cool air diminishes because of the abatements of the velocity and "sweeping time" of the air jet over the subjects. But at the same time, the increased frequency offsets a certain diminution. So with the interaction of the two sides, different rotative speed is preferred in different thermal conditions. It can be seen in Fig. 8 that 3.4 rpm is preferred in condition A, and 6.8 rpm in condition B.

Table 3 lists the velocities sensed by the subjects at different rotative speeds of the outlet. Standard deviations are also listed in parentheses.

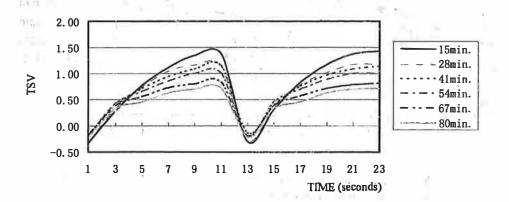


Fig. 2 TSV during two rotative periods of the outlet at different testing time in experimental condition A.

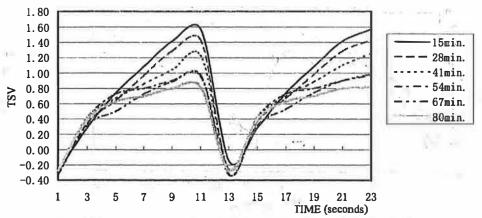


Fig. 3 TSV during two rotative periods of the outlet at different testing time in experimental condition B.

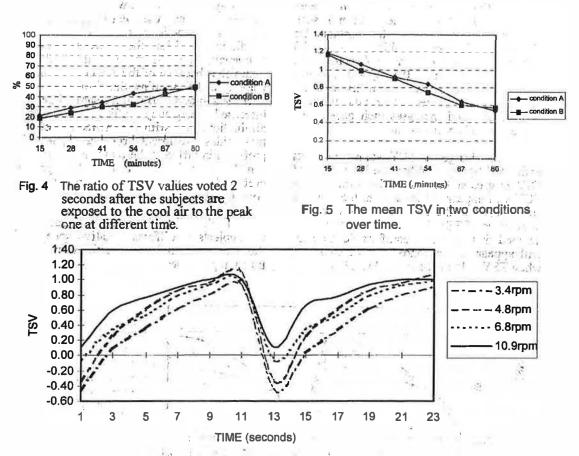


Fig. 6 TSV during the two rotative periods of the outlet at the different rotative speeds in experimental condition A.

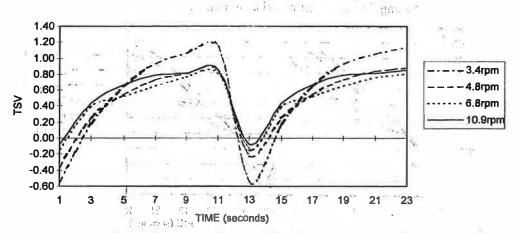


Fig. 7 TSV during the two rotative periods of the outlet at the different rotative speeds in experimental condition B.

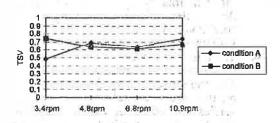


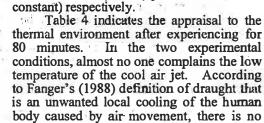
Fig. 8 Mean TSV at different rotative speeds in two experimental conditions.

Table 3 Velocities sensed by the subjects at different rotative speeds of the outlet.

Vj	1.5m/s	1.7m/s
3.4rpm	0.99 (0.195)	1.09 (0.122)
4.8rpm	0.81 (0.217)	0.91 (0.106)
6.8rpm	0.58 (0.121)	(0.104)
10.9rpm	0.45 (0.198)	0.55 (0.154)

#### **DISCUSSION**

Fig. 9 and 10 show the comparison of the measured TSV at 15 and 80 minutes and **PMV** in two experimental conditions. PMV1 is much higher than the peak value of TSV, which indicates the cool air cuts down the human body's heat stress, and improves the subjects' thermal conditions significantly. PMV2 is also greater than the minimum of measured TSV, which can be explained by the overshoot happened when human body is exposed to temperature step. PMV1 and



correspond to the conditions of (Ta

constant, Vs = 0) and (Tjt = constant, Vs =

complaint about draught.

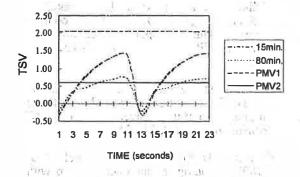


Fig. 9 Comparison of the measured TSV at 15 and 80 minutes and Fanger's PMV in condition A.

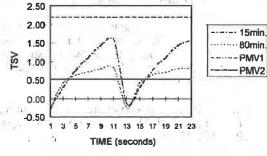


Fig. 10 Comparion of the measured TSV at 15 and 80 minutes and Fanger's PMV in condition B.

Table 4 Appraisal to the thermal environment

rable 4 Appraisar to the thermal environment								
	Can you accept this		what do you think of the		What do you think of			
	thermal environment?		temperature of cool air?			the velocity of the jet?		
	Yes	No	OK	High	Low	OK	High	Low
condition A	87.5%	12.5%	50%	50%	none	37.5%	12.5%	50%
condition B	75%	25%	62.5	37.5%	none	none	25%	75%

## CONCLUSIONS

- Non-isothermal and intermittent cool air jet can be used to improve the subjects' thermal conditions significantly and increase their acceptance of the thermal environment.
- From the hot environment to the dynamic environment caused by the non-isothermal and intermittent cool jet, there is a course of adaptation during which the sensitivities to the cool air is diminishing, and the cool effect is reducing.
- The sensed velocities are variable at

- different rotative speeds of the outlet. And under different air temperature conditions, the thermal sensation is varied with the speed of rotation.
- There is no complaint about the draught caused by the intermittent cool jet.
- The present study is performed with the relative humidity below 50%, further studies are recommended to study the effect of non-isothermal intermittent cool jet in the muggy condition. Likewise, more thermal conditions are recommended for study

#### NOMENCLATURE

TSV thermal sensation vote (seven-point scale) **TCV** thermal comfort vote (five-point scale) **PMV** predicted mean vote (seven-point scale)

F

Ta

= distance from the outlet (m)

= rotative frequency of the outlet (rpm)

= room air temperature (°C)

= average air temperature at the outlet of the jet (°C)

= axial temperature of the air jet at the distance where it first meets the person( $\mathfrak{C}$ ) axial velocity of the air jet at the distance where it first meets the person (m/s) Vs sensed velocity by the subjects; averaged for the pools of the subjects (m/s)

# REFERENCES

Azer, N. Z. and Nevins, R. G. (1974) Physiological effects of locally cooling the head in 95 °F and 75% RH environment. ASHRAE Transactions, 80(1), 1-8.

Burton, D. R., Robeson, K. A. and Nevins R. G. (1975) The effect of temperature on preferred air velocity for sedentary subjects dressed in shorts. ASHRAE Transactions, 81(2), 157-168.

Fanger, P. O. Air turbulence and sensation of draught. (1988) Energy and buildings, 1988(12), 12-39.

ISO. 1984. ISO Standard 7730, Moderate thermal environments-Determination of the @ PMV and PPD indices and specification of the conditions for thermal comfort. Geneva:

> warmen restlanted in a

000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 1000 | 100

International Organization for Standardization.

Melikov, A. K., Halkjaer, L., Arakelian, R. S. and Fanger, P. O. (1994) Spot cooling -- part (1): Human responses to cooling with air jets. ASHRAE Transactions, 100(2), 476-499.

Rohles, F. H., Konz, S. A. and Jones, B. W. (1983) Ceiling fans as extenders of the summer comfort envelope. ASHRAE Transactions, 89(1), 245-262.

Scheatzle, D. G., Wu, H. and Yellott, J. (1989) Extending the summer envelop with ceiling fan in hot, arid climates. ASHRAE Transactions, 95(1), 269-280.