

A review of pollutants and sources of concern and performance-based approaches to residential smart ventilation

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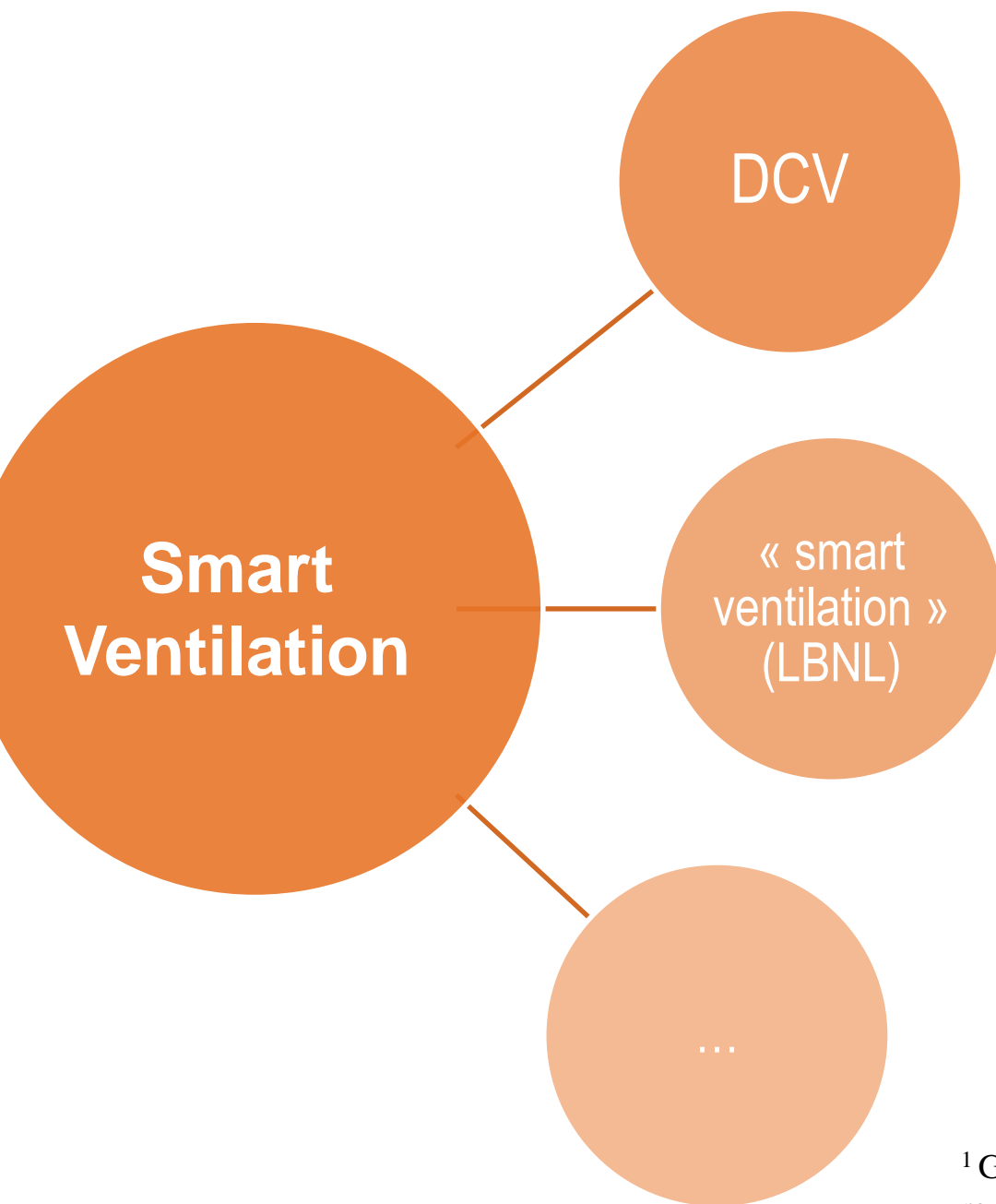
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Outline

- Scope : smart ventilation strategies
- Relevant parameters for smart ventilation
- Performance-based approaches in 5 standards and regulations
- Perspectives

Our scope : smart ventilation strategies

- Smart ventilation : modulation of ventilation airflows in response to several factors
 - ⇒ reduce ventilation energy use and cost while maintaining the same indoor air quality (IAQ) as a continuously operating system, or better
- From a literature review (not a market survey)
 - *In-press : Guyot, G., Sherman, M.H., Walker, I., 2017. Residential smart ventilation: a review. Lawrence Berkeley National Laboratory. In-press*



- Over 30 years old
- Widely used in countries as FR, BE, NT
- Mostly CO₂ or humidity based with a wide variety of systems and strategies
- IAQ : various results
- Energy savings : -26% + 60% ¹
- **Performance-based approaches**

- RIVEC prototype (Sherman and Walker, 2011)
- ACH = f(outdoor conditions, utility peak loads, occupancy, operation of other air systems)
- IAQ maintained, sometimes improved
- Energy savings : >40%, 500-7000 kWh/year/household
- **Performance-based approach = Equivalence principle**

¹ Guyot, G., Sherman, M.H., Walker, I., 2017. Residential smart ventilation: a review. Lawrence Berkeley National Laboratory.

Relevant parameters for smart ventilation

■ Pollutants of concerns

- Borsboom, W., De Gids, W., Logue, J., Sherman, M., Wargocki, P., 2016. TN 68: Residential Ventilation and Health, AIVC Technical Note 68.

Table 6: Priority pollutants in the indoor residential environment for consideration in making ventilation standards

| PRIORITY POLLUTANTS FOR CHRONIC EXPOSURE (RANKED BY POPULATION IMPACT) | POTENTIAL ACUTE EXPOSURE CONCERNS |
|---|--------------------------------------|
| Particulate matter | Acrolein |
| Mould/ moisture | Chloroform |
| Formaldehyde | Carbon Monoxide |
| Acrolein | Formaldehyde |
| | NO ₂ |
| | PM _{2.5} |

Relevant parameters for smart ventilation

■ Pollutants of concerns

- Borsboom, W., De Gids, W., Logue, J., Sherman, M., Wargocki, P., 2016. TN 68: Residential Ventilation and Health, AIVC Technical Note 68.

■ Odors, CO₂ and humidity, temperature

- Correlation between them / with other types of indoor pollutants ?
- No consensus about the conclusions !

■ Occupancy

Relevant parameters for smart ventilation

- **Also an issue of availability and reliability of sensors :**
 - Performance, size, extend of signal conditioning, reliability, robustness, maintainability, cost
- **Only some CO₂ and humidity sensors seems accurate and reliable enough with affordable costs**
- **But not only a question of sensors !**
 - also control strategies algorithms, regulation type, localization of sensors,

Performance-based approaches in some countries

Context

- A number of ventilation standards and national regulations with an allowance for smart ventilation strategies and/or DCV systems in residential buildings
 - Simultaneously, EP regulations with the opportunity to claim credit for savings from such systems
-
- ⇒ Performance-based approaches defined and required for smart ventilation strategies
 - ⇒ DCV strategies used at massive scale, notably in France and in Belgium, for more than 30 years

Compliance required in some State regulations in US and Canada

| Ventilation Equivalence method | Person in charge | Calculated IAQ indicators | Credit in EP-calculation | Minimum airflow | Market |
|---|---|--|--------------------------|---|------------------|
| Single zone modeling $\Delta t < 1h$ Constant pollutant emission rate | The manufacturer, specifier or designer | No specifically defined pollutant Yearly average relative exposure $R < 1$ At each time-step $R_i < 5$ | Rare | Can be null if the total airflow rate equivalence is required over any 3-hour periods | Some DCV systems |

Relative Exposure R(t)

$$R(t) = \frac{C(t)}{C_{eq}} =$$

To avoid peak exposure

$$R_i = \frac{Q_{tot}}{Q_i} + \left(R_{i-1} - \frac{Q_{tot}}{Q_i} \right) e^{-Q_i \Delta t / V_{space}} < 5 \quad \text{if } Q_i \neq 0$$

Equation 15

$$R_i = R_{i-1} + \frac{Q_{tot} \Delta t}{V_{space}} < 5 \quad \text{if } Q_i = 0$$

Where Q_{tot} is the minimum constant ventilation rate calculated according to section 4.1 of the ASHRAE 62.2,
 Q_i is the real-time airflow in the variable mechanical ventilation system at time step i ,
 Δt is the time-step used in the calculation,
 V_{space} is the volume of the space.

France

Avis techniques

| Performance-based approach | Person in charge | Calculated IAQ indicators | Credit in EP-calculation | Minimum airflow | Market |
|---|------------------|--|---|--|--|
| Multi-zone modeling $\Delta t = 15$ min Conventional entry data: meteorological, homes geometries, airleakage distribution, occupancy, ...) | The manufacturer | Per room, over the heating period : 1/ CO_2 cumulative exposure indicator $E_{2000} < 400.000 \text{ ppmh}$ 2/Number of hours $T_{RH>75\%} < 600 \text{ h}$ in kitchen, 1000 h in bathrooms, 100 h in other rooms | Average equivalent exhausted airflow (m^3/h) can be implemented in the EP-calculation ~ -40% | Switch off not allowed 10-35 m^3/h according to the number of rooms in the building | > 30 years 23 DCV systems with agreements (mostly RH controlled) > 90% new homes |

$$E_{2000} = \sum_{t=0}^T C_{\text{CO}_2 > 2000}(t) * t < 400\,000 \text{ ppm.h}$$

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| Performance-based approach | Person in charge | Calculated IAQ indicators | Credit in EP-calculation | Minimum airflow | Market |
|--|------------------|---|---|-----------------|--|
| Multi-zone modeling $\Delta t = 40$ s Conventional entry data: meteorological, homes geometries, occupancy, ...) | The manufacturer | Per room, over the year : 1/CO ₂ cumulative exposure indicator $E_{1600} < 500.000$ ppmh 2/ Yearly average CO ₂ concentration < 900 ppm | Yearly average ventilation airflow could be implemented in the EP-calculation | / | 3 DCV systems with agreements (recent procedure) |

2017 : Towards a performance-based approach for every new building equipped with any type of ventilation system, using a software and some conventional data

| Former performance-based/equivalence approach | Person in charge | Calculated IAQ indicators | Credit in EP-calculation | Minimum airflow | Market |
|---|------------------|---|--|-----------------|--|
| Multi-zone modeling $\Delta t = 5$ min Conventional entry data both deterministic and stochastic | The manufacturer | Per person, over the heating period, At least equal that the worst performing reference system : 1/ CO_2 cumulative exposure indicator E'_{950} 2/Monthly average RH > 80% on critic thermal bridges from December 1st to March 1st 3/Exposure to a tracer gas emitted in toilets and in bathrooms | An energy saving coefficient f_{reduc} is extrapolated and can be implemented in the EP-calculation | / | 34 DCV systems with agreements (mostly CO_2 controlled) |

No more ATG-E since 2015

- 2014: DCV systems considered as mature enough to be directly integrated in the EP-calculation method
- A study (Caillou et al., 2014b) evaluated the 35 systems gaining the ATG-E through an advanced equivalence method
- 2016: only the energy saving coefficients f_{reduc} given in the tables of an Ministerial Order (Moniteur Belge, 2015) can be used directly in the EP-calculation
 - Sensors accuracy requirement
 - Minimum airflows over 10% of the minimum constant airflow for each room

| Type of detection in dry spaces | Type of regulation of air inlets in dry spaces | Local detection in humid spaces with regulation of air outlet Local regulation | Local detection in humid spaces with regulation of air outlet No local regulation | Other or no detection in humid spaces |
|--|--|---|--|---------------------------------------|
| CO ₂ -local : at least a sensor in each dry space | Local | 0.35 | 0.38 | 0.42 |
| | 2 zones (night/day) or more | 0.41 | 0.45 | 0.49 |
| CO ₂ - partially local : at least a sensor in each bedroom | Central | 0.51 | 0.56 | 0.61 |
| | Central | 0.60 | 0.65 | 0.70 |
| CO ₂ - partially local : at least a sensor in the main bedroom + at least a sensor in the living room | 2 zones (night/day) or more | 0.43 | 0.48 | 0.53 |
| CO ₂ -central : at least a sensor in the exhaust duct(s) | Central | 0.75 | 0.81 | 0.87 |
| | Central | 0.81 | 0.87 | 0.93 |
| Occupancy-local : at least a sensor in each dry space | Local | 0.54 | 0.60 | 0.64 |
| | 2 zones (night/day) or more | 0.63 | 0.67 | 0.72 |
| Occupancy-partially local : at least a sensor in each bedroom | Central | 0.76 | 0.82 | 0.88 |
| | Central | 0.87 | 0.93 | 1.00 |
| Occupancy-partially local : at least a sensor in the main bedroom + at least a sensor in the living room | 2 zones (night/day) or more | 0.66 | 0.72 | 0.78 |
| Other or no detection in dry spaces | Central | 0.87 | 0.93 | 1.00 |
| | No, local, per zone, or | 0.90 | 0.95 | 1.00 |

The Netherlands

Standard NEN 8088 & a complementary performance-based approach

| Standard and performance-based approaches | Person in charge | Calculated IAQ indicators | Credit in EP-calculation | Minimum airflow | Market |
|---|---|---|--|---|--------------------------------|
| Correction factors are given in the standard NEN 8088 for quite a few DCV systems | The person involved in EP-calculation (standard approach) | Per person, over the heating period : Cumulative CO ₂ exposure over 1200 ppm: | Given correction factors directly used in the EP-calculation | A function of the number of type of occupants | 37 DCV systems with agreements |
| OR | OR | | OR | | |
| A complementary performance-based approach uses a multi-zone modeling, in a semi-probalistic approach | the manufacturer (performanc-based approach) | LKI ₁₂₀₀ < 30.000 ppm.h | New correction factors are calculated | | |

$$LKI_{1200} = \sum_{t=0}^T \left(\frac{C_{CO_2>1200}(t) - 1200}{1000} \right) * t < 30 \text{ kppm.h}$$

Equation 22

Where $C_{CO_2>1200}(t)$ is the absolute concentration at which an occupant is exposed at t time-step, if it is higher than 1200 ppm, or 800 ppm above the outdoor concentration.

Conclusions

- Performance indicators used in performance-based approaches for smart ventilation strategies are related to CO₂ exposure and condensation risk (exc. ASHRAE 62.2)
- As many smart ventilation systems types than regulations and performance-based methods, because manufacturers have to adapt their systems...

- **Smart ventilation strategies success is not ready to end ...**
 - Two recently European published directives (Ecodesign n°1253/2014 EcoLabeling n°1254/2014) : toward a generalization of DCV and balanced heat recovery systems at the 2018 horizon
- **Can we use this background for the definition of a performance-based approach at the design stage of every new dwellings equipped with any type of ventilation system?**

Thank you for your attention !

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■ Towards an health performance-based approach ?

- As proposed in Sherman, M.H., Walker, I.S., Logue, J.M., 2012. Equivalence in ventilation and indoor air quality. HVAC&R Research 18, 760–773. doi:10.1080/10789669.2012.667038

$$DALY = \sum_i \text{Concentration}_i * UDE_i$$

Equation 23

$$DALY_{limit} = \sum_i \text{Standard}_i * UDE_i$$

Equation 24

| Compound | UDE $\left[\frac{\mu DALYS}{year * person} * \frac{m^3}{\mu g} \right]$ | Chronic Standard $\left[\frac{\mu g}{m^3} \right]$ | Chronic Standard damage $\left[\frac{\mu DALYS}{year * person} \right]$ |
|---------------------|--|---|--|
| Priority Pollutants | | | |
| 1,3 Butadiene | 0.02 | 0.06 | 0.001 |
| 1,4-dichlorobenzene | 0.03 | 0.91 | 0.024 |
| Acetaldehyde | 0.3 | 3.7 | 0.96 |
| Acrolein | 190 | 0.02 | 3.7 |
| Benzene | 0.08 | 0.34 | 0.025 |
| Formaldehyde | 6.8 | 1.7 | 11.4 |
| Naphthalene | 0.47 | 0.29 | 0.14 |
| Nitrogen Dioxide | 0.70 | 40 | 27 |
| PM _{2.5} | 500 | 15 | 7,500 |
| Other contaminants | | | |
| Ammonia | 0.23 | 200 | 46 |
| Ozone | 1.4 | 147 | 200 |
| Crotonaldehyde | 1.02 | N/A | N/A |

Table 11: Indoor air contaminants – UDE_i and Standard_i values in order to implement the IAQ equivalence principle according to Equation 23 and Equation 24 , source : (Sherman et al., 2012)